APPENDIX E2

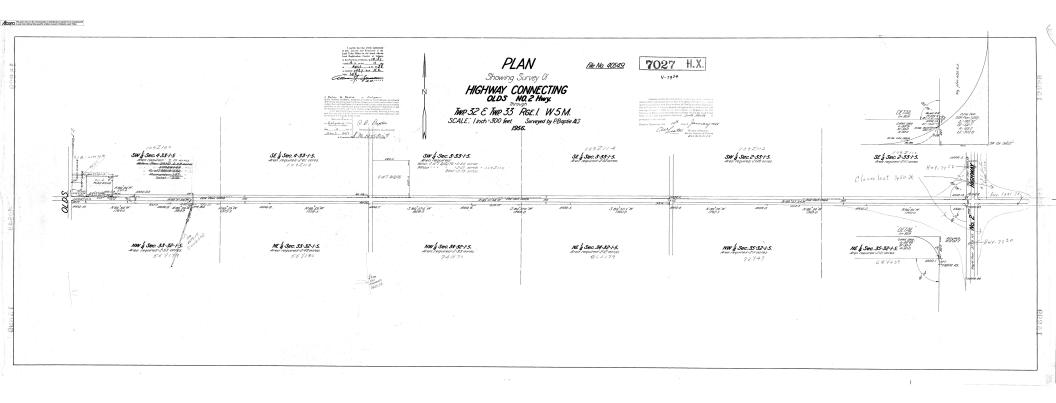
Land Titles -

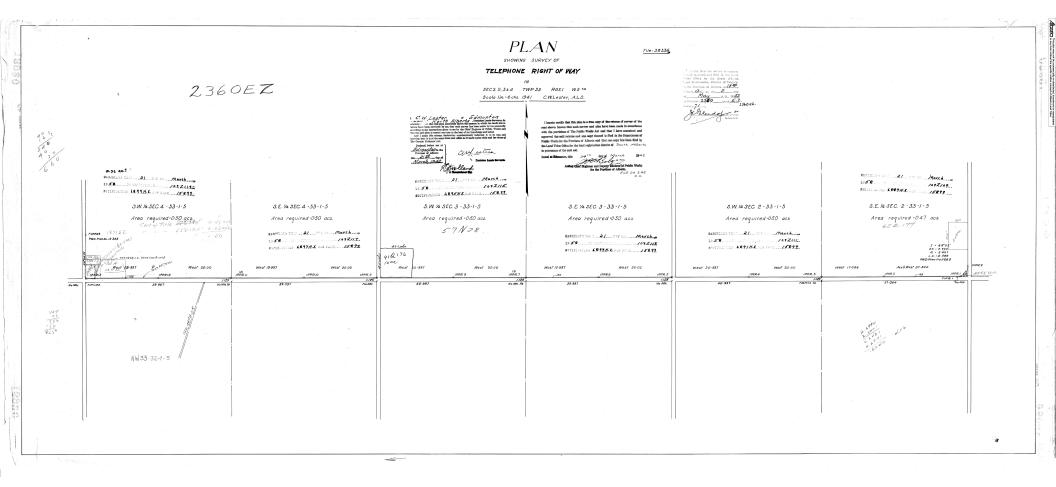
Survey

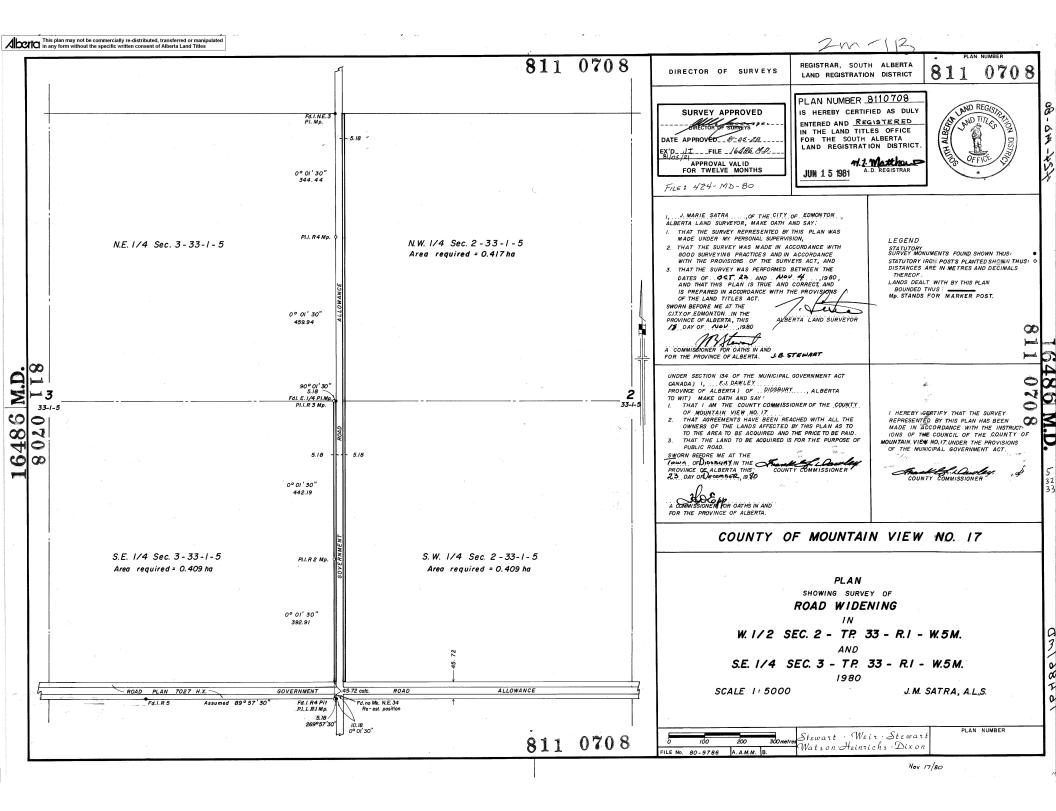


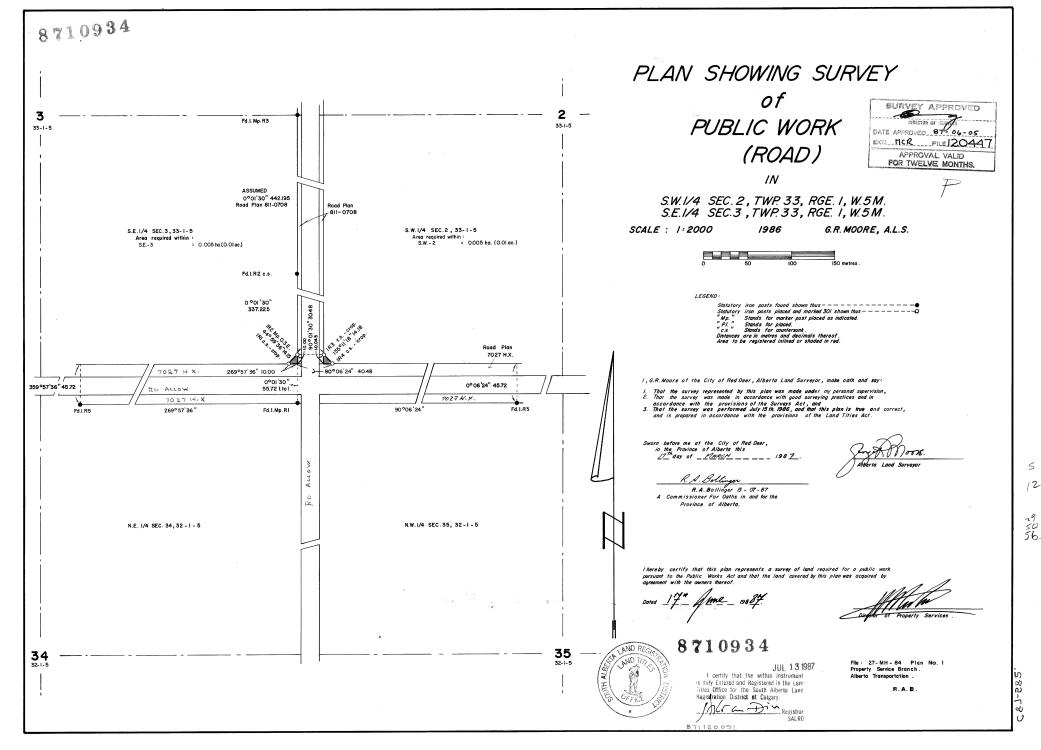


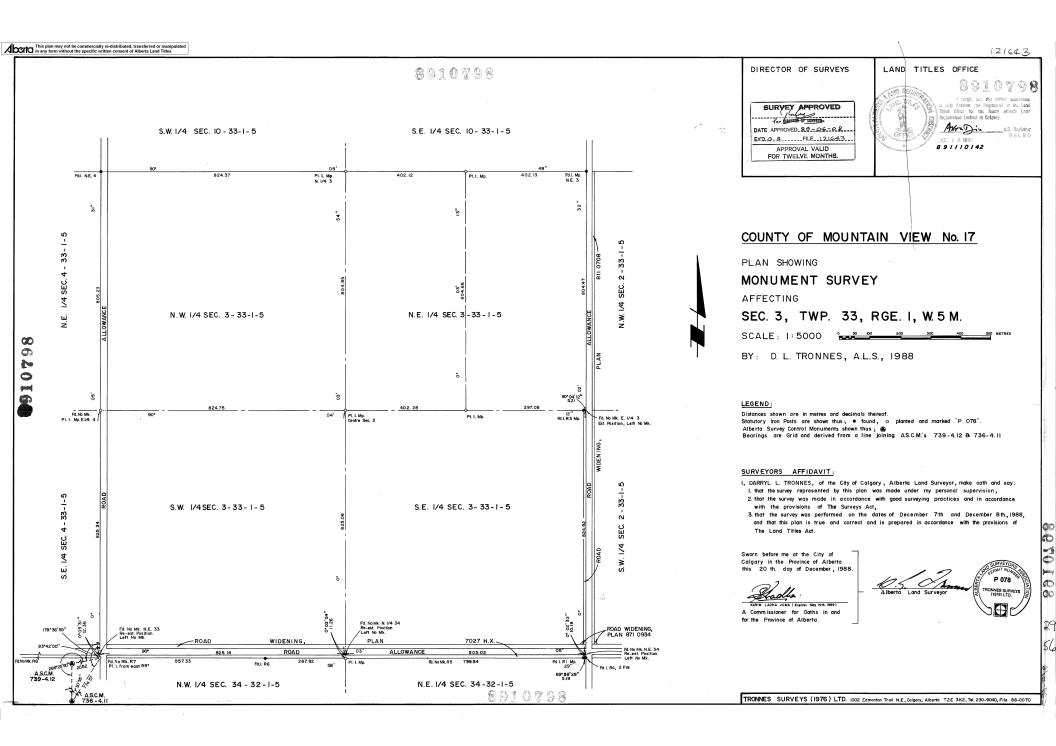
Environmental and Remediation Services Inc.

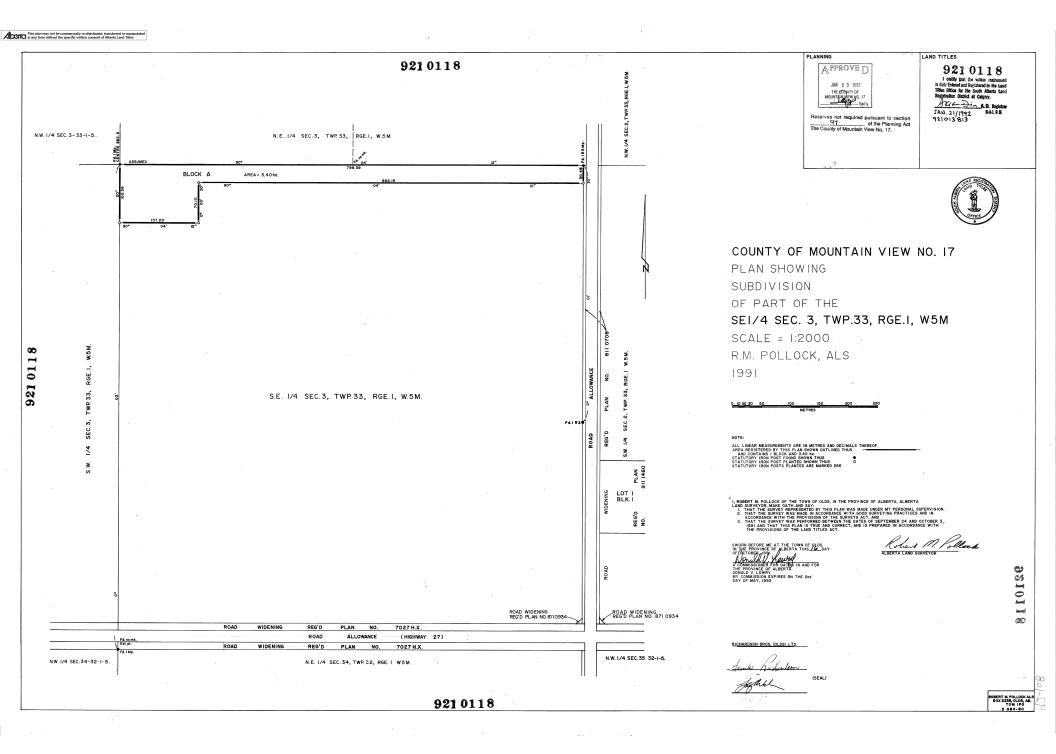






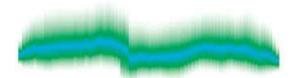






APPENDIX F

Company Records





Environmental and Remediation Services Inc.

APPENDIX F1

Macintosh –

Geotechnical Report





Environmental and Remediation Services Inc.

GEOTECHNICAL EVALUATION MOUNTAIN VIEW MEADOWS BUSINESS PARK AND RESIDENTIAL COMMUNITY MOUNTAIN VIEW COUNTY- ALBERTA

April, 2008

M•L 3899

GEOTECHNICAL EVALUATION MOUNTAIN VIEW MEADOWS BUSINESS PARK AND RESIDENTIAL COMMUNITY MOUNTAIN VIEW COUNTY, ALBERTA

SUBMITTED TO:

<u>.</u> -

MMM Group Limited Calgary, Alberta

PREPARED BY:

McIntosh•Lalani Engineering Ltd. Calgary, Alberta

April, 2008

M•L 3899

<u>M•L 3899</u>

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1.0 INTRODUCTION

This report presents the results of a geotechnical evaluation conducted by McIntosh-Lalani Engineering Ltd. (M•L) for the proposed Mountain View Meadows development in Mountain View County, Alberta. This evaluation was undertaken at the request of Mr. John Berry, P.Eng. of MMM Group Ltd. The objective of this evaluation was to assess the general subsurface soil conditions within the site and provide geotechnical construction guidelines for the development. The scope of work is summarized as follows:

- Drill thirty five (35) boreholes to a depth of 9 metres on an approximate 250 m grid and install PVC standpipes in each to allow future monitoring of groundwater conditions across the site.
- Drill six (6) boreholes to a depth of up to 3.0 metres across the two S.E. quarters for assement of the suitability of the site for weeping tile fields.
- Measure groundwater elevations in the monitoring wells, approximately 1 week after drilling.
- Undertake laboratory testing, as necessary, to aid in determining the geotechnical engineering properties of the soils.
- Prepare a geotechnical evaluation report providing the findings of the site investigation, analysis and geotechnical recommendations for the design and construction of the development.

The following sections present our understanding of the project and the results and recommendations of the geotechnical investigation.

2.0 **PROJECT DETAILS**

It is our understanding that the project is composed of the development of approximately four contiguous quarter sections of land immediately northwest of Highway 2 and Highway 27, east of Olds, Alberta, into a business park and residential community. Based on conceptual drawings supplied by MMM group, the land is understood to be partitioned into approximately 500 residential lots and 190 acres of commercial and light industrial lots,

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As such, development of the land is understood to involve stripping and grading of the site and construction of the underground utilities and roadways. This report serves to present the results of the field drilling program, laboratory testing and recommendations with regard to the above noted construction issues.

3.0 SITE DESCRIPTION AND TOPOGRAPHY

The subject lands are composed of portions of Sections 2 and 3, Township 33, Range 1, west of the 5th meridian, which lie immediately to the northwest of Highways 2 and 27.

The lands are presently utilized for mainly agricultural and grazing purposes, with several acreage style houses. Topographically, the lands are flat to rolling, with little overall vertical relief and several small potholes and sloughs.

4.0 FIELD AND LABORATORY WORK

The fieldwork consisted of drilling forty one (41) subsurface investigation boreholes from February 15 to February 25, 2008, using a solid stem auger drill rig contracted from Beck Drilling & Environmental Services Inc. of Calgary. Standard Penetration Testing (SPT) and Pocket Penetrometer measurements were taken at select depths in the boreholes to aid in classifying the soil strengths and disturbed soil samples were collected for laboratory testing Slotted PVC standpipes were installed in all boreholes to allow for future monitoring of groundwater levels.

The boreholes were drilled on an approximate 250 m grid spaced more or less evenly across the lands. The borehole locations were surveyed and marked prior to drilling by MMM Group Ltd, on the grid pattern noted above. It should be noted, however, that BH's 36 to 41, representing the percolation field testholes, were not drilled in their surveyed locations. The approximate location of the boreholes are shown on the attached Figure No. 1, and the borehole logs are presented in Appendix A.

The laboratory test program included natural moisture contents, soluble sulphate concentrations, Atterberg Limits and grain size distribution determination on select soil samples. The result of these tests are discussed throughout the text of this report and are shown on the attached borehole logs.

5.0 SURFICIAL GEOLOGY AND GROUNDWATER CONDITIONS

5.1 Soils

The general subsurface soil stratigraphy of the site consists of surficial organic topsoils overlying glacial till soils atop sedimentary bedrock. In addition, shallow deposits of sandy sediments were encountered in several boreholes, which may be a relic of historic wetland or sloughy areas.

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Organic topsoil was encountered in all forty one boreholes, ranging in thickness from 75 mm to 405 mm. The average depth of organic topsoil encountered during drilling was approximately 165 mm. Only negligible depths of organic browns were encountered, and the topsoil was composed almost entirely of black loam, which is typical for tilled fields. Organic browns may be encountered in the undisturbed treed areas of the northern quarter.

Underlying the topsoil, glacial tills composed of silts and silty clays were encountered in the majority of the boreholes. In six of the forty one boreholes, silt and sand deposits were encountered beneath the topsoil, which may either be a glacial deposit or possibly sediments from historic wetland or slough areas. Where encountered, the sandy sediments were described as compact and dry to damp, and typically extended to a depth of 1.5 m to 2.5 m below existing grade.

Underlying these sandy deposits, or directly underlying the topsoil, glacial till was typically encountered. The till was generally composed of a compact and dry to damp silt at the surface, underlain by a silty clay till. The silt till extended to a depth of 1 to 2 metres below existing grade, although in many cases the silt material was absent and the silty clay till was encountered directly underlying the topsoil. The silty clay till was stiff in consistency, being damp and medium plastic with traces of sand and gravel throughout. Lenses and pockets of sand and silt were also encountered throughout the silty clay till body. The glacial material extended to either sedimentary bedrock or beyond the depth of drilling in all boreholes.

Sedimentary bedrock was encountered in only four boreholes, at depths ranging from 7 to 8 metres below existing grade. In addition, bedrock was encountered at a depth of only 3 metres below grade in BH-3, which may represent a piece of rafted sandstone or boulder. Auger refusal was met, and the exact nature of the shallow bedrock in this area was not determined. Where encountered, the bedrock was composed of hard sandstone and siltstone.

A more detailed soil description of each borehole is presented in the borehole logs in Appendix A.

At the time this report was prepared, information regarding the subsurface stratigraphy was available only at discrete borehole locations. Conditions were extrapolated and interpolated from the borehole locations to develop the following recommendations. Adequate monitoring should be provided during construction to confirm that these assumptions are reasonable. If conditions are encountered during construction that do not agree with the borehole information, M-L should be allowed to revise our recommendations.

5.2 Groundwater

Groundwater seepage was only encountered during drilling in one of the forty one boreholes, BH-23, in a deep sand lense encountered at a depth of 8.7 m below grade. The remainder of the boreholes were largely dry upon completion.

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Groundwater measurements were taken on March 7, 2008, at which point the groundwater depth ranged from 2.9 m below grade to dry to a depth of 9.1 m below grade. This corresponds to a groundwater elevation ranging from 1015.1 m to 1006.2 m ASL.

The groundwater measurements are presented on Table No. 1, attached.

6.0 DISCUSSION AND RECOMMENDATIONS

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Design recommendations presented in this report are based on the assumption that an adequate level of inspection will be provided during construction and that construction will be carried out by a suitably qualified contractor, experienced in underground utility installation and earthworks. An adequate level of inspection is considered to be:

- for earthworks full time monitoring and compaction testing.
- for underground utility installation and backfilling full time monitoring and compaction testing.
- for foundation bearing inspections inspection by qualified geotechnical engineering personnel.

Inspection should be carried out by suitably qualified persons, independent of the contractor. The purpose of providing an adequate level of inspection is to check that recommendations, based on the data obtained at discrete borchole, are relevant to other areas of the site.

6.1 Construction Excavation and Temporary Dewatering

The composition and consistency of the site soils are such that conventional hydraulic excavators should be suitable to remove the majority of the site soils. Relatively shallow bedrock was encountered in some boreholes, at depths as shallow as 3 m in BH-3. This may represent a piece of rafted bedrock or an isolated boulder; however, if encountered during deep utility construction it may pose difficulties. Use of rippers or pneumatic chipping tolls may be required in such an instance.

All excavations should have no more than 1.5 m of vertical wall before backsloping at a maximum gradient of 1H:1V is required. Deeper excavations encountering the sand or silt seams may require additional backsloping or shoring if excessive seepage is noted during construction. Excavations should be inspected by a geotechnical engineer if such conditions are encountered during utility construction.

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Due to the shallow groundwater encountered in areas of the site, excavations may encounter groundwater infiltration and require dewatering. The volume of seepage is anticipated to be relatively limited, and sumps equipped with submersible pumps would be considered a feasible method of dewatering in these instances.

6.2 Site Grading

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. | Some cuts and fills may be required within the proposed development. All organic topsoil and vegetation should be removed from areas to be filled. The backfill should be placed in uniform lifts compacted to a minimum of 98 percent of Standard Proctor Density at a moisture content in the range of optimum to 3 percent above optimum. For the most part, conventional methods of site grading using scrapers are considered to be feasible on this site.

The building footprint of large commercial or light industrial facilities may include most, if not all, of the available lot space. Therefore, we recommend that the entire lot be treated as a building envelope. Alternatively, the commercial lots should be left ungraded.

6.3 Pipe Support

Over the majority of the site, we do not anticipate any difficulties with regard to the pipe support. Conventional methods for pipe support are considered feasible.

Clay plugs should be used around utilities founded in predominately silt or sand soils. The frequency and locations of plugs should be determined once utility and site grades have been finalized.

6.4 Foundations

Based on the results of the geotechnical investigation, conventional shallow foundations in conjunction with slabs-on-grade are considered feasible for residential structures.

All foundations placed on fill soils should be protected by installation of weeping tile subdrains around all footings. This should include the rear frost wall of any walkout units. In addition, all backfill placed around foundation walls should be properly moisture conditioned and compacted to a minimum of 95 percent Standard Proctor Density.

We recommend that residential footings be designed for a soil bearing capacity of 100 kPa. Bearing certificates should be prepared for all footings placed on fill by qualified geotechnical engineering personnel.

Footings within heated structures should be founded at a depth of 1.4 m below grade and for unheated structures at a depth of 2.1 metres grade to protect against the effects of frost heaving.

April 14 2008

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Both conventional shallow strip and spread footing and deep pile foundation systems are considered feasible for commercial or industrial buildings in the area. However, due to the wide variance in potential building types, sizes and loads, we recommend that independent geotechnical investigations be performed for each lot by the owner prior to construction.

6.5 Weeping Tile Fields

Six additional boreholes (BH's 36 to 41) were advanced across the middle of the Phase 1 area, which is comprised of the south half of Section 2. The final location and layout of the weeping tile fields has not yet been determined, therefore, these boreholes are only intended to give a general idea of the suitability of the site for weeping tile fields.

Soil conditions in the six boreholes noted above consisted of the surficial organic topsoils overlying 1 to 2 metres of silt till atop silty clay glacial till. Groundwater was not encountered during drilling, or within 3 m of the surface during subsequent monitoring.

Soil Index Properties

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Hydrometer Testing (BH's 36-4)

	Maximum	Minimum	Average
Clay Fraction	27 %	13 %	17.6 %
Silt Fraction	51 %	40 %	45.8 %
Sand Fraction	47 %	31 %	36.5 %

Atterberg Limit Testing (Across Whole Site)

	Maximum	Minimum	Average
Plastic Limit	13.3	10.1	10.5
Liquid Limit	39.0	.25.5	36.2
Plasticity Index	26.7	13.6	24.4

Based on these tests, on average, the site soils consist of a low to medium plastic sandy silt with some clay, with a wide variation in sand content. Given these results, the site soils appearsuitable for construction of weeping tile fields. Percolation testing should be conducted across the site during the late spring or summer, once the field layouts have been determined to confirm these results.

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6.6 Concrete Type

Laboratory testing of select soil samples has shown the concentration of water soluble sulphates to be up to 1.1 percent. Therefore, all concrete elements in contact with the site soils should be designed for a S-2 exposure class.

7.0 DESIGN AND CONSTRUCTION GUIDELINES

Recommended general design and construction guidelines are provided in Appendix B, under the following headings:

- Backfill Materials and Compaction
- Construction Excavations
- Shallow Foundations

These guidelines are intended to present standards of good practice. Although supplemental to the main text of this report, they should be interpreted as part of the report. Design recommendations presented herein are based on the premise that these guidelines will be followed. The design and construction guidelines are not intended to present detailed specifications for the work, although they prove useful in the preparation of such specifications. In the event of any discrepancy between the main text of this report and Appendix B, the main text should govern.

8.0 LIMITATIONS

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Recommendations presented herein are based on a geotechnical evaluation of the findings in forty one (41) boreholes. The conditions encountered during the fieldwork are considered to be reasonably representative of the site. If, however, conditions other than those reported are noted during subsequent phases of the project, M•L should be given the opportunity to review our current recommendations in light of new findings.

This report has been prepared for the exclusive use of MMM Group Ltd. and their agents for specific application to the development described in this report. It has been prepared in accordance with generally accepted soil and foundation engineering practices. No warranty is expressed or implied.

9.0 CLOSURE

We trust information presented herein meets with your present requirements. If you have questions or require additional geotechnical services please contact our office.

M•L 3899

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McIntosh•Lalani Engineering Ltd.

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Lee Martin, E.I.T.

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REPMIT TO PRACTICE MOINTOSH LALANI BINGINEERING LTD. Signature Cum Date PERMIT NUMBER: P 6482 The Association of Professional Engineers, Geologists and Geophysicists of Alberta



A.W. McIntosh, P.Eng. Senior Project Engineer

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LIST of FIGURES

S 2

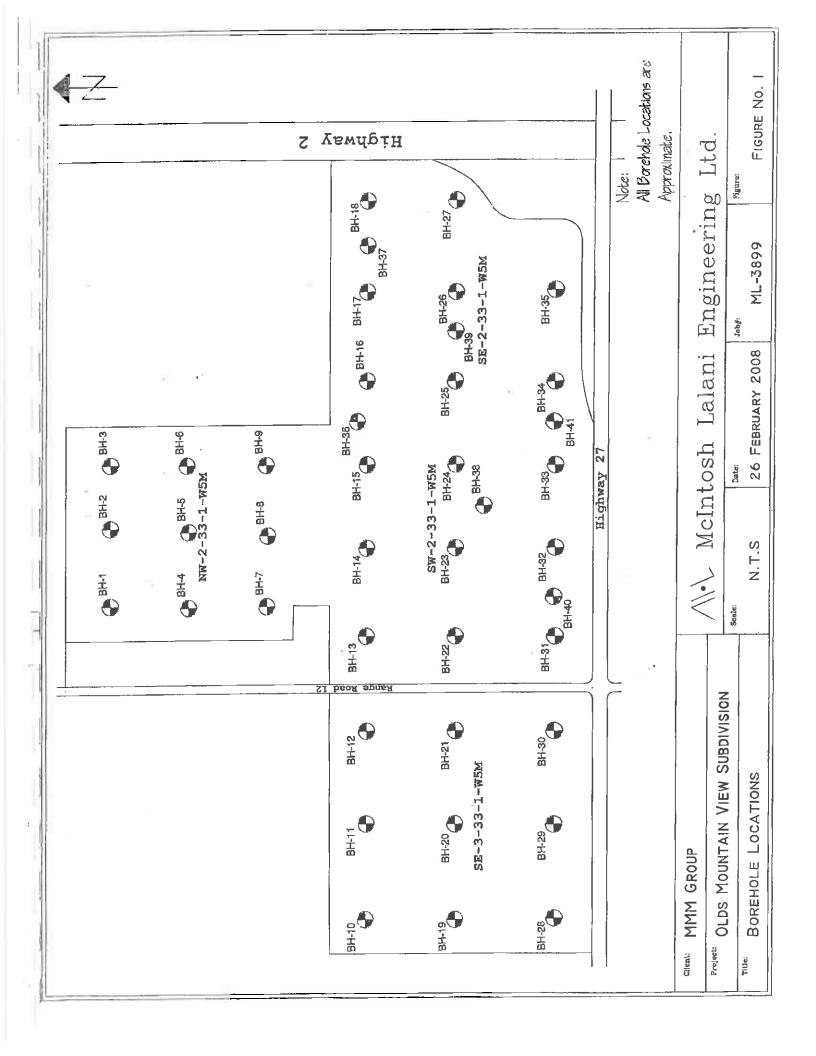
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LIST of FIGURES

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TABLES

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McIntosh Lalani

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GROUNDWATER SUMMARY SHEET

PROJECT NAME Olds Mountain View Subdivision

OJECT NUMBER 3899				Sheet 1
Borehole	Surface Elevation	Date of Reading	Depth to Groundwater	Groundwate Elevation
1	1017.16	3/7/2008	7.05	1010.11
		4/2/2008	5.09	1012.07
2	1015.60	3/7/2008	3.42	1012.18
		4/2/2008	3.46	1012.14
3	1015.45	3/7/2008	2.96	1012.49
		4/2/2008	2.98	1012.47
4	1016.98	3/7/2008	6.8	1010.18
		4/2/2008	3.98	1013
5	1014.55	3/7/2008	2.93 .	1011.62
		4/2/2008	2.95	1011.6
6	1015.44	3/7/2008	4.64	1010.8
		4/2/2008	3.64	1011.8
7	1017.34	3/7/2008	2.86	1014.48
		4/2/2008	2.78	1014.56
8	1014.49	3/7/2008	4.15	1010.34
		4/2/2008	3.02	1011.47
9	1015.10	3/7/2008	3.69	1011.41
		4/2/2008	3.24	1011.86
10	1018.42	3/7/2008	3.35	1015.07
		4/2/2008	3.45	1014.97
11	1018.20	3/7/2008	3.64	1014.56
		4/2/2008	3.76	1014.44
12	1020.11	3/7/2008	7.78	1012.33
		4/2/2008	7.15	1012.96
13	1016.90	3/7/2008	7.09	1009.81
		4/2/2008	5.82	1011.08
14	1015.46	4/2/2008	8	1007.46
16	1014.34	3/7/2008	4.8	1009.54
		4/2/2008	3.52	1010.82
17	1015.81	3/7/2008	4.44	1011.37
		4/2/2008	3.92	1011.89
18	1010.77	3/7/2008	2.51	1008.26
		4/2/2008	2.65	1008.12
19	1020.28	3/7/2008	8.01	1012.27
		4/2/2008	6.84	1013.44
20	1018.75	3/7/2008	5.57	1013.18
		4/2/2008	4.93	1013.82
21	1020.06	3/7/2008	8.03	1012.03
		4/2/2008	7.8	1012.26
23	1014.75	3/7/2008	8.01	1006.74
		4/2/2008	7.45	1007.3
24	1014.29	3/7/2008	7.8	1006.49

McIntosh Lalani

GROUNDWATER SUMMARY SHEET

CLIENT MNIM Group

PROJECT NAME Olds Mountain View Subdivision

ECT NUMBER 3899	3899 DATE <u>4/14/2008</u>			
				Sheet 2
Borehole	Surface Elevation	Date of Reading	Depth to Groundwater	Groundwate Elevation
24	1014.29	4/2/2008	5.28	1009.01
25	1013.98	3/7/2008	6.83	1007.15
		4/2/2008	4.14	1009.84
27 ·	1010.62	3/7/2008	3.61	1007.01
		4/2/2008	3.77	1006.85
28	1019.36	3/7/2008	5.3	1014.06
		4/2/2008	5.35	1014.01
29	1018.68	3/7/2008	5,53	1013.15
	•	4/2/2008	5.34	1013.34
32	1015.21	3/7/2008	8.98 ·	1006.23
		4/2/2008	8.93	1006.28
33	1013.57	4/2/2008	5.82	1007.75
34	1014.53	3/7/2008	7.66	1006.87
		4/2/2008	6.34	1008.19
35 .	1013.00	4/2/2008	6.29	1006.71

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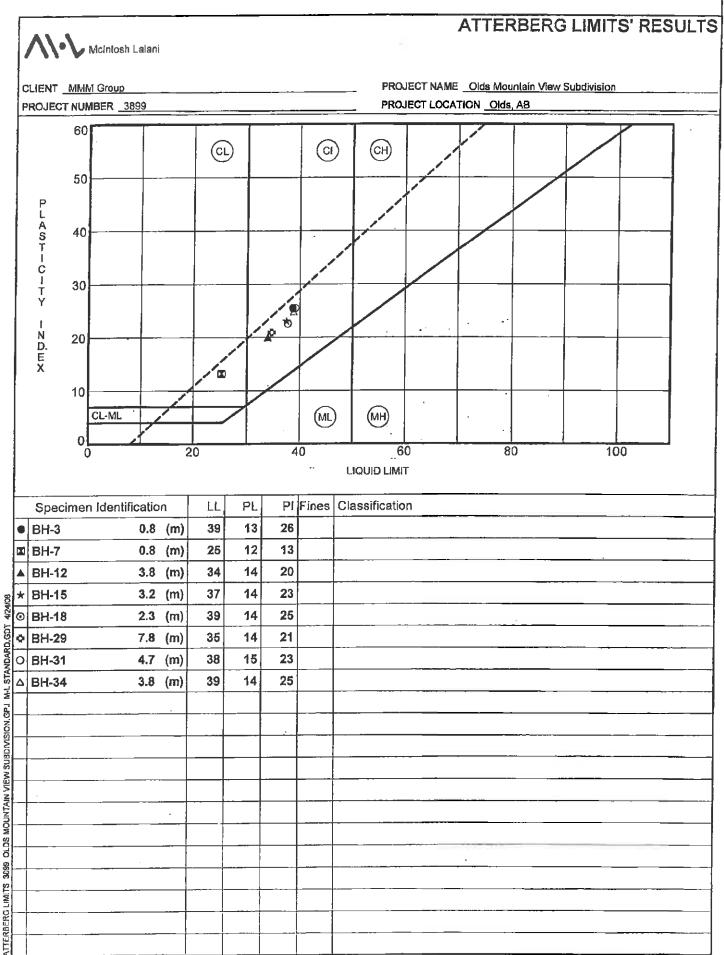
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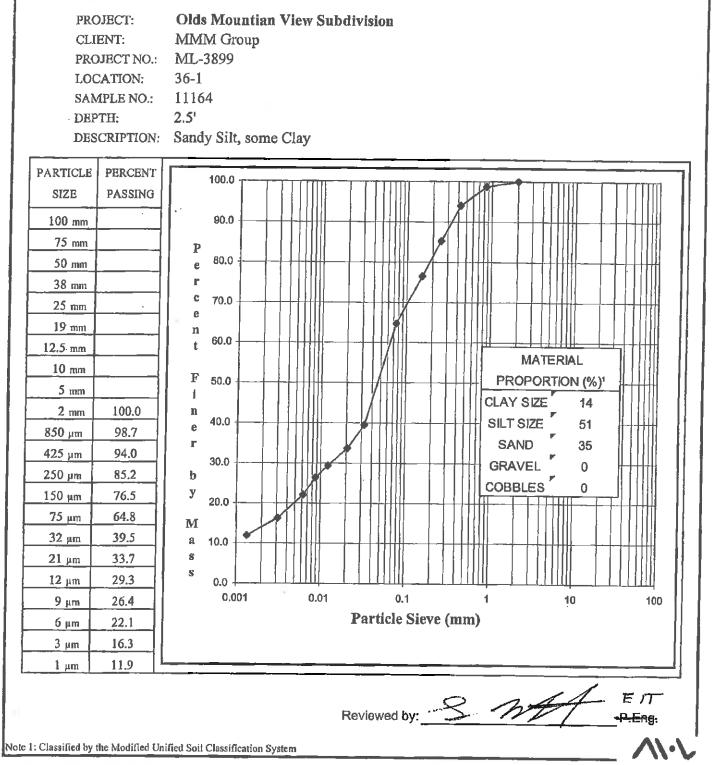
LAB TESTING



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STANDARD TEST METHOD FOR PARTICLE SIZE

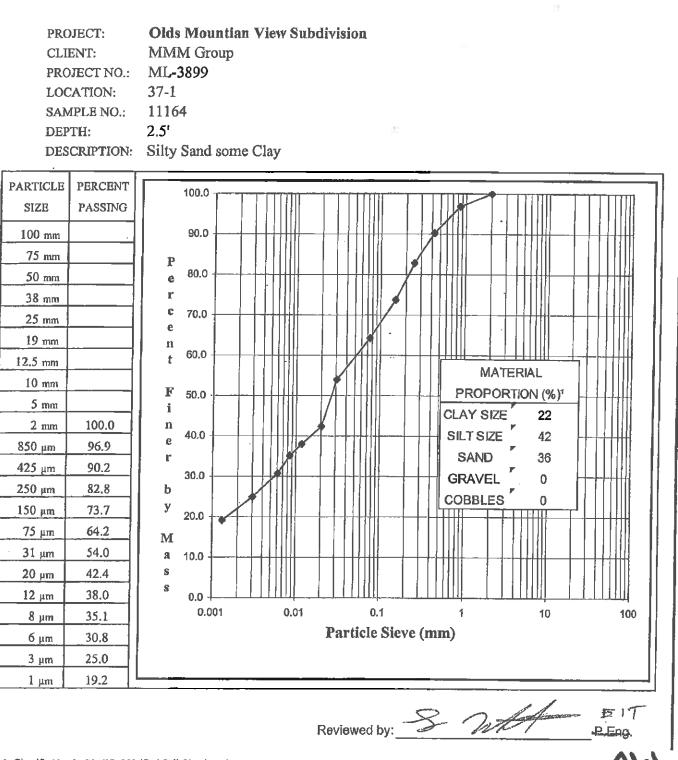
(Test Method ASTM D422)



Data presented hereon is for the sole use of the stipulated client. ML is not responsible, nor can be held liable, for use made of this report by any other party, with or without the knowledge of ML. The lesting services reported herein have been performed by an ML technician to recognized industry standards, unless otherwise noted. No other warranty is made. These data do not include or represent any interpretation or opinion of specification compliance or material suitability. Should engineering interpretation be required, ML will provide it upon written request.

STANDARD TEST METHOD FOR PARTICLE SIZE

(Test Method ASTM D422)



Note 1: Classified by the Modified Unified Soil Classification System

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STANDARD TEST METHOD FOR PARTICLE SIZE

(Test Method ASTM D422)

CLII PRO LOC SAM DEP DES PARTICLE SIZE 100 mm 75 mm 38 mm 38 mm 25 mm 19 mm 12.5 mm 10 mm 5 mm 2 mm 850 μm 425 μm 250 μm 150 μm 150 μm 150 μm 31 μm 20 μm	CRIPTION: PERCENT PASSING 	Olds Mountian View Subdivision ML-3899 38-2 11164 7.5 Silty Sand some Clay	
6 µm	38.0	11	
1 μm	25.0		
I: Classified by		Reviewed by: Show Fit P.Eng.	

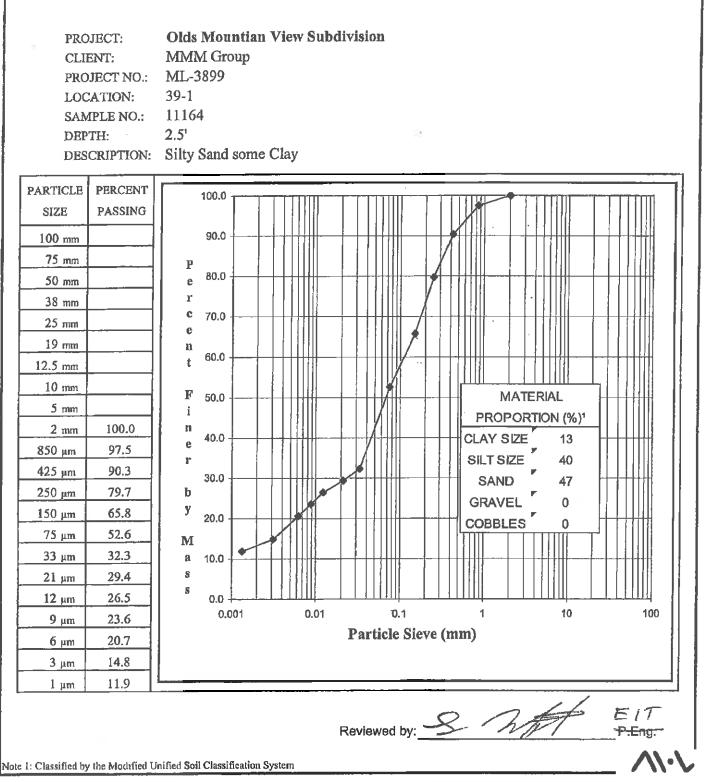
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STANDARD TEST METHOD FOR PARTICLE SIZE

(Test Method ASTM D422)



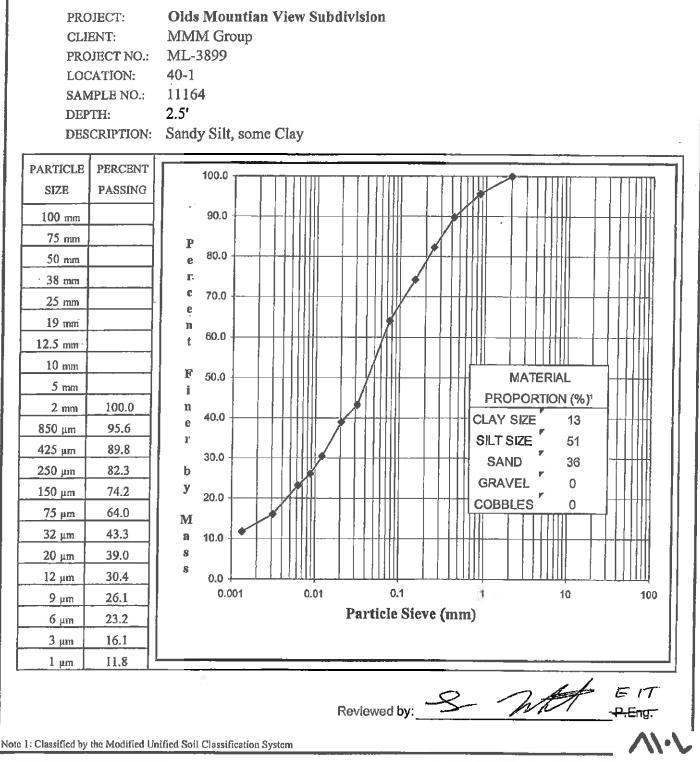
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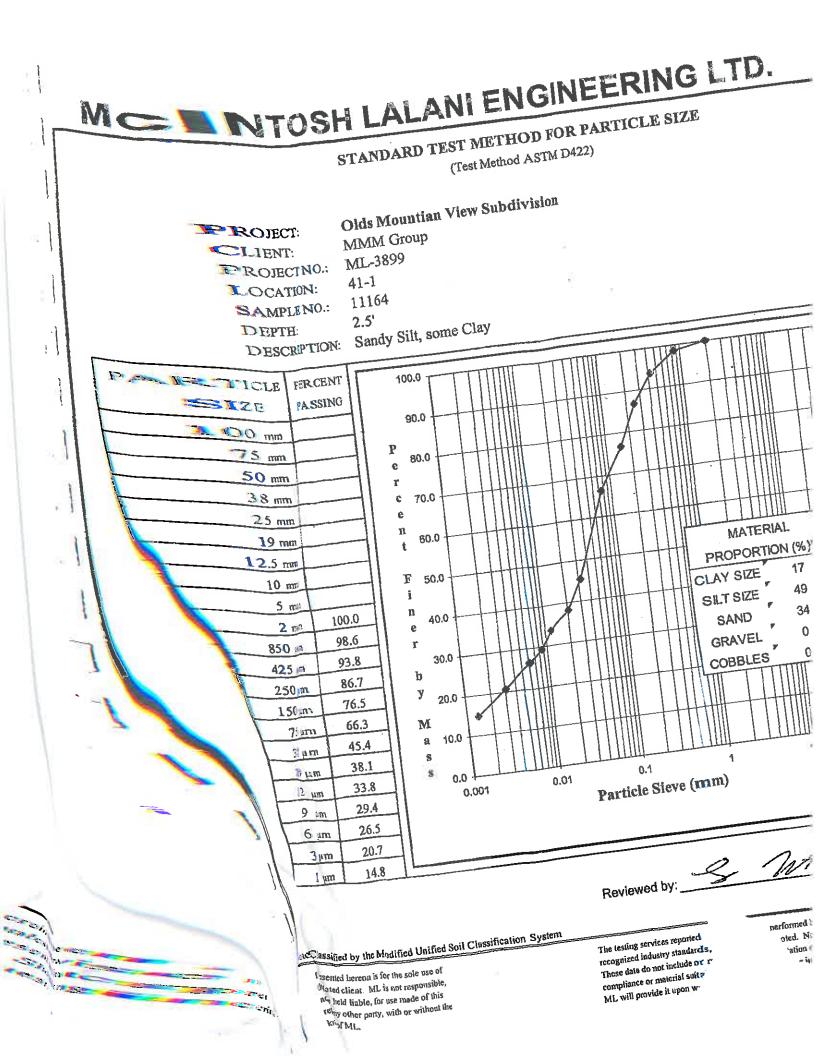
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STANDARD TEST METHOD FOR PARTICLE SIZE

(Test Method ASTM D422)



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APPENDIX A

BOREHOLE LOGS

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APPENDIX A

BOREHOLE LOGS

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Pro	ject: Old	Is Mountain View Subdivision			-		rmalion: g & Enviro	nmen	tal Servic	35		le No.:1 No.:3899		
Clie	ent: MM	VI Group	·				S-Auger		(4) 001 110			n:1017.16		
	LE TYP		COR	E SAN			SPT SAMPI	.6	GR	AB SAMPLE	AUGER SA		RECOVE	ERY
_	FILL TY		PEA	GRAV	ÆL.		SLOUGH		GR	сит 🛛	ORILL CUT		D	
Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO	uscs	BLOWS /150 mm		MLC.			30 40	OTHER DATA	SLOTTED PIEZOMETER	
		Topsoil - approx. 100mm thick. Silty Clay (Till) - stiff, damp, some sand, trace gravel, medium plast trace coal, light brown. - cobbles. - trace sand, medium brown. - trace oxides. Silt - dense, damp, weathered, so siltstone, medium grey. Silty Clay (Till) - stiff, damp, trace gravel, medium plastic, medium grey. END OF HOLE at a depth of 9.1m 25mm PVC standpipe installed to depth of 9.1m with 6.1m slotted. Explored to the state of t	me	1-1 1-2 1-3 1-4	IPSL CI CI							{SO ₄] = 0.03%		101 101 101 101 101 101 1010 1009
0		upon completion. Water Levels: March 07, 2008 - 7.05 M April 02, 2008 - 5.09 M			i	•								1007
		a					<u></u>	<u></u>		minile Kon		alian Darih. 20 4		
AA	1	McIntosh Lalani I Calgary, AB	Engineer	ring					ewed By: Doi ewed By: L			elion Depth: 30 ft on: 2/25/2008	-	
N 14.										CORT INTERNAL	• DBBCU	VIL CLEUR COUD		

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Proj	ject: Olds	s Mountain View Subdivision			rilling Info	-		aments	I Service				le No.:2 No.:389	9		
Clie	nt: MMM	Group			ME 55 S			arriering					n:1015.			-
	LE TYPE		CORE	_]SPT S		E	GRA	B SAMPLE		UGER S/			ECOV	/
	FILL TYP		PEA GF	RAVEL.]slou			GRO	UT		RILL CUT	TINGS	SANE		•
Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO USCS	BLOWS /150 mm	PLAS	ITIC	M.C.	LIQUID		OW COUNT 20 30	40		THER	SLOTTED	
	Ale ale	Topsoil - approx. 100mm thick.		TPS		1	0 2	20 30	40	<u>BD 1</u>	KETPEN (kP 60 240	320				
		Sandy Silt (Till) - compact, damp trace clay and gravel, light brown	· _	2-1 MLS		• • • • • •	1.2		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,							
2		04 01 (TH) and been		2-2	9-10-18		3									
		Silty Clay (Till) - stilf, damp, trace sand and gravel, medium plastic, trace coal and oxides, medium brown.		2-3							· · · · · · · · · · · · · · · · · · ·	•				
-3 ¥		 trace sandstone. sand lenses throughout. 		.4	4-10-13		¥.							ŝ		
-4 		- sand tenses throughout.	2	2-5												
-5		- poor recovery, rock in spoon.		-6 cı	8-16-18	6.8										
2 6			2	-7							•					11111
		- medium grey.		-8	4-14-15	· · · · · · · · · · · · · · · · · · ·	16									
7 7				-9	2-8-9											~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
		Bedrock (Siltstone) - strong, dry, platey, medium grey. - hard drilling.	2.	BE												11111111
		END OF HOLE at a depth of 9.1m 25mm PVC standpipe installed to depth of 9.1m with 6.1m slotted. I upon completion.), a			4 · · · · · · · · · · · · · · · · · ·									Ŧ	
		Water Levels: March 07, 2008 - 3.42 M April 02, 2008 - 3.46 M														
		McIntosh Lalani Calgary, AB	Engineerin	l 1g	1	<u></u>				ninik Ken ee Martîn			letion Dep I on: 2/25/			-

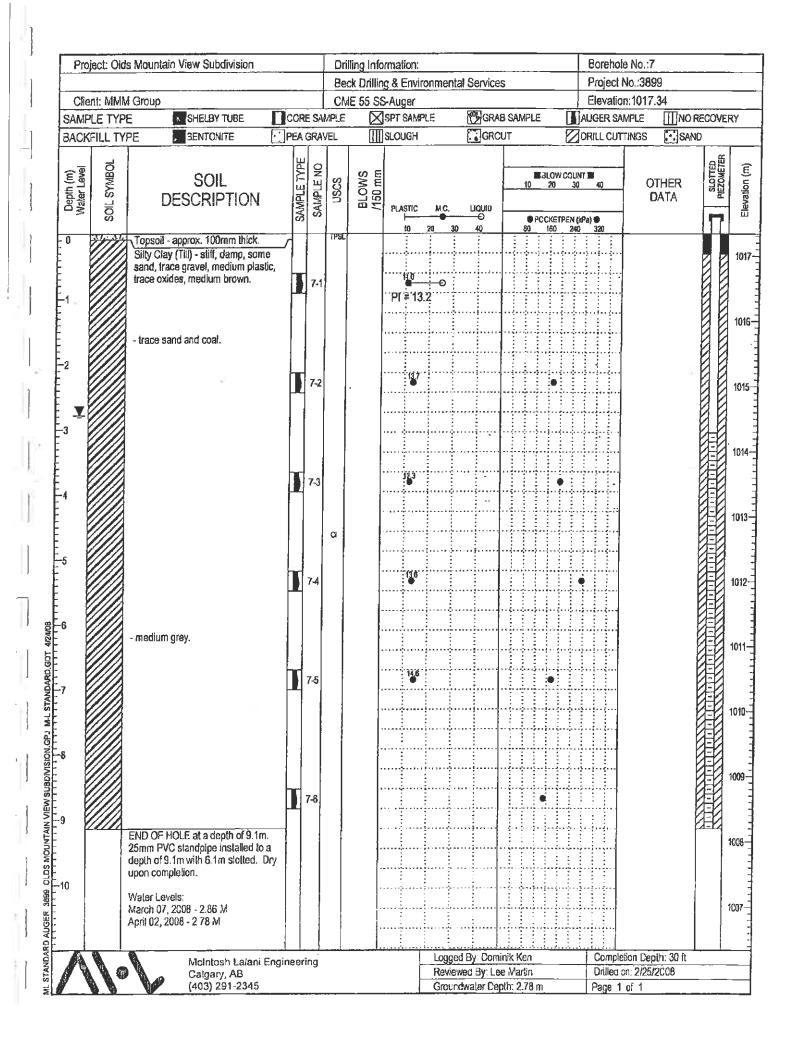
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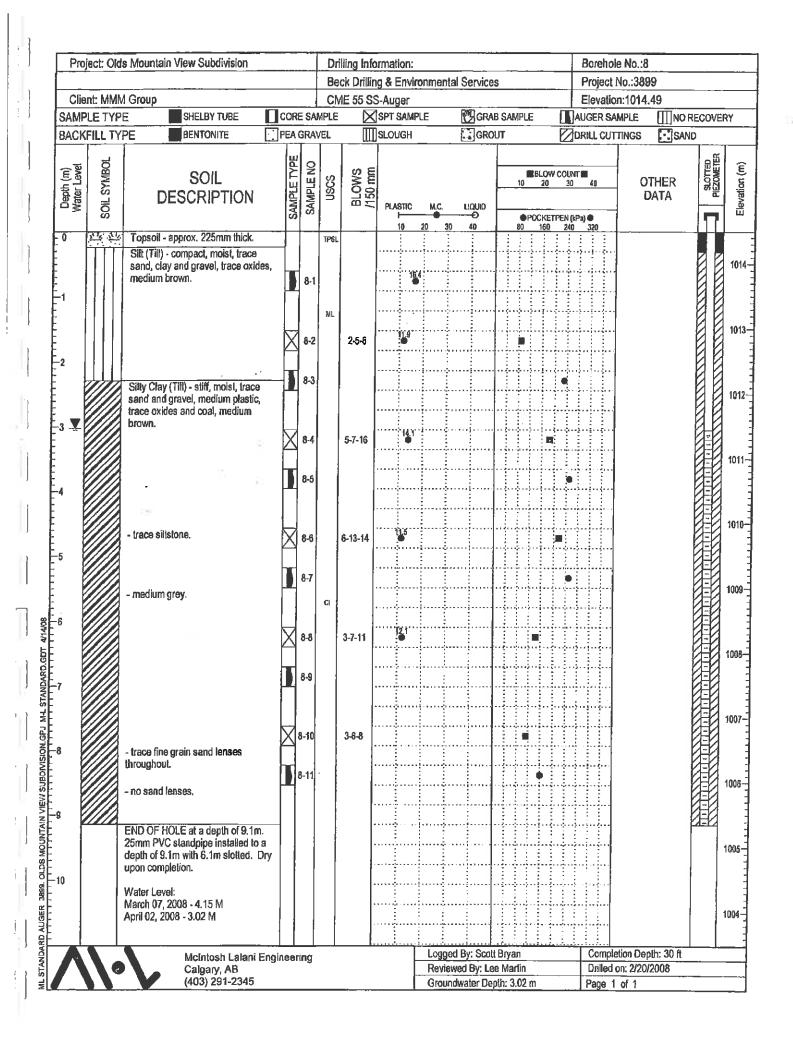
Project:	Olds N	Iountain View Subdivision				rilling Infi						Borehole		
									nmenta	al Service:	s		No.:3899	
Client: N					_	ME 55 S			-	all on a	B SAMPLE	AUGER SA	n:1015.45 MPLE NI	000
SAMPLE		SHELBY TUBE			AMPL		SPT 8		E	GRO				
BACKFILL	TYPE	BENTONITE	<u>. []</u> PE/	A GH		<u>Ш</u>]]SLOU	IGH		Le GRU			11NGO [[]]3/	(ND
Depth (m) Water Level		SOIL DESCRIPTION		SARIFLE ITTE	USCS	BLOWS /150 mm			M.C. 0 30	11QUID 	■ 3LOW C 10 20 ● PCCKETPE 80 160		other Data	
-0	*	Topsoil - approx. 100mm thick.			TP8	9L	+		<u></u>			240 320		-
		Silty Clay (Till) - stiff, damp, son and, trace gravel, medium play race oxides and coal, medium rown.	ne (stic,	3	-1			0 ⁹ ∓ 25.8	2	o				
-2		sand lense.		3	-2 -2			127				*	:	
_3 ⊻	Ē	ledrock (Sandstone) - strong, c ght brown.	iry,		BE	-								
-4	2 d	ND OF HOLE at a depth of 4.3 5mm PVC standpipe installed epth of 4.3m with 2.4m slotted. pon completion.	loa	3	3									
-6	N	Vater Levels: farch 07, 2008 - 2.96 M pril 02, 2008 - 2.98 M												
-7														
-8														
-9														1
-10														

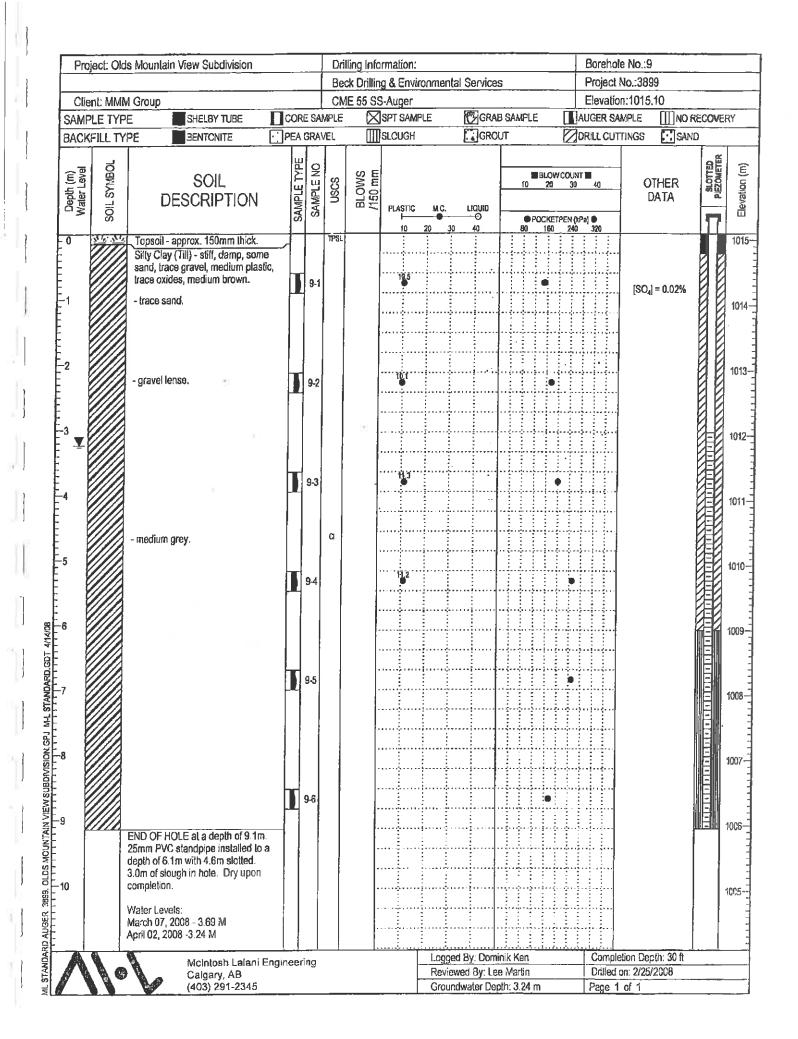
Client: MMM Group Edwalen: 1016 38 SAMPLE TYPE Internet of the second s	Proj	ect: Old	s Mountain View Subdivision		_			rmation: n & Envir	oment	al Service	s	Borehole Project N	e No.:4 No.:3899		
SAMPLE TYPE SHELBY TUPE CORE SAMPLE CORE SAMPLE <thcore sample<="" th=""> <thcore sample<="" th=""></thcore></thcore>	Clie	nt MMA	1 Group									+			
BACKFILL TYPE ENTONITE PERCAWEL ENDONCH CORL CUTTINGS CONTINUE Backfill SOIL DESCRIPTION SOIL DESCRIPTION Backfill DATA Backfill DESCRIPTION DESCRIPTION SOIL DESCRIPTION Backfill Backfill DATA Backfill DESCRIPTION DESCRIPTION Backfill Backfill DATA DATA Backfill DESCRIPTION Backfill Backfill Backfill DATA DATA Backfill DATA Backfill Backfill Backfill DATA DATA Backfill DATA Backfill Backfill Backfill DATA DATA Backf				COR	E SAN				E	GRA	B SAMPLE	· · · · · · · · · · · · · · · · · · ·		ECOVE	RY
Image: Solution of the soluti							Π	SLOUGH		GRO	UT Z	DRILL CUT)	
0 100 100 100 100 100 100 100 100 100 100	Depth (m) Water Level	SOIL SYMBOL		SAMPLE TYPE	SAMPLE NO	USCS	BLOWS /150 mm	I			POCKETPEN	0 40 (MP⊐)●		PIEZOMETER	
and, face gravel, low to madium plastic, trace works, light brown. a -1 -trace sand and coal, spoon bouncing on a cobile. -etif. a -a a </td <td>0</td> <td></td> <td>Topsoil - approx. 150mm thick</td> <td></td> <td></td> <td>TPSL</td> <td></td> <td>10</td> <td>20 30</td> <td></td> <td>00 100 2</td> <td>40 320</td> <td></td> <td></td> <td>F</td>	0		Topsoil - approx. 150mm thick			TPSL		10	20 30		00 100 2	40 320			F
- lack shift and toda, spont ↓ <	-1		sand, trace gravel, low to mediur	n l	4-1			102							10
4 4 6-10-16 • • 5 4-6 4-6 - • • 6 - - - - • • 7 4-8 4-7 - • • • 8 REFUSAL on a boulder at a depth of 7.9m. with a thread by or 0.9m with a thread by	-2		bouncing on a cobble.	X			bouncing					•			1
4	3		949 X.	X	4-4		6-10-16	12.5							1
5 4.7 4.7 4.8 4.8 3.4.7 4.8 3.5.10 7 8 REFUSAL on a boulder at a depth of 7.9m with 6.1m slotted. Dry upon completion. Water Levels: March 07, 2008 - 6.80 M April 02, 2008 - 3.98 M	4 Y		2 2 - 1 (m)		4-5	a						•			1
 medium grey. 4.8 4.8 4.9 4.9 4.9 4.10 3.5-10 REFUSAL on a boulder at a depth of 7.9m with 6.1m stotled. Dry upon completion. Water Levels: March 07, 2008 - 6.80 M April 02, 2008 - 3.98 M 	5			X	4-6		4- 9 -13	138							1
REFUSAL on a boulder al a depth of 7.9m. 25mm PVC standpipe installed to a depth of 7.9m with 6.1m stotted. Dry upon completion. 3.5-10 Water Levels: March 07, 2008 - 6.80 M April 02, 2008 - 3.98 M					4-7										1
REFUSAL on a boulder at a depth of 7.9m. 25mm PVC standpipe installed to a depth of 7.9m with 6.1m slotted. Dry upon completion. Water Levels: March 07, 2008 - 6.80 M April 02, 2008 - 3.98 M			- medium grey,				3-4-7	13.8							
REFUSAL on a boulder at a depth of 7.9m. 25mm PVC standpipe installed to a depth of 7.9m with 6.1m slotted. Dry upon completion. Water Levels: March 07, 2008 - 6.80 M April 02, 2008 - 3.98 M	7				4-10		3-5-10								1
March 07, 2008 - 6.80 M April 02, 2008 - 3.98 M	3		7.9m. 25mm PVC standpipe installed to a depth of 7.9m with												1
	•		March 07, 2008 - 6.80 M							•••••					1
	0														10
A Completion Depth: 23 ft			1					<u></u>							

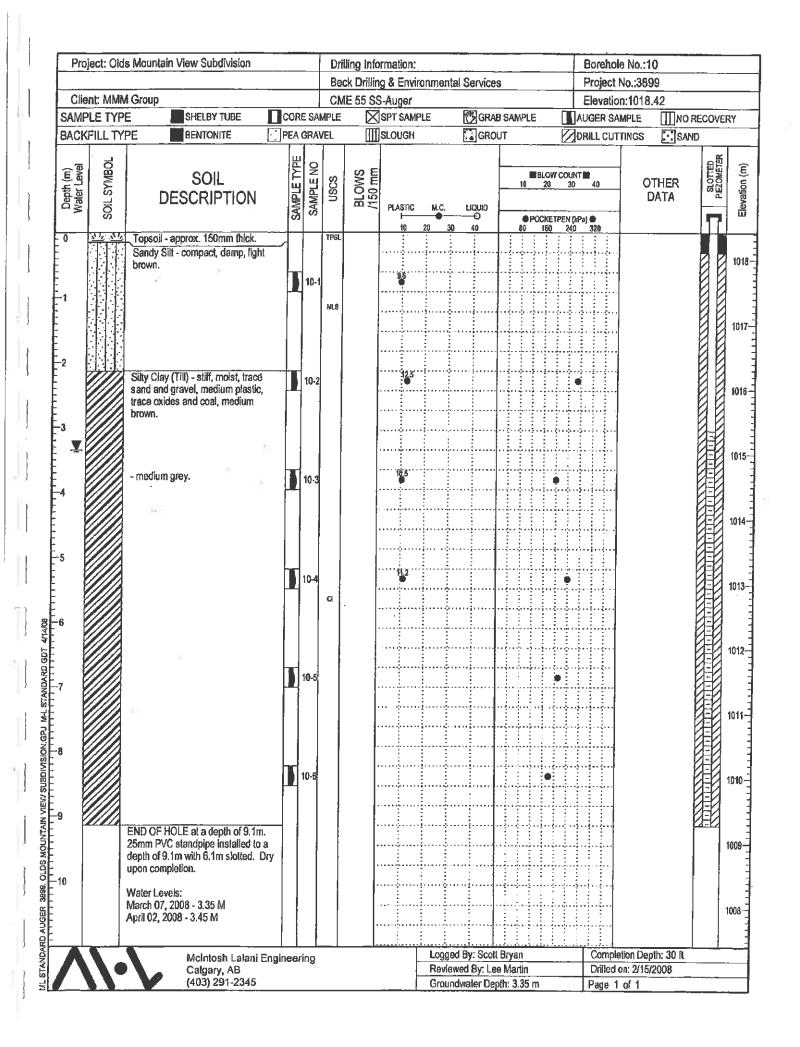
Citeri: MAM Group CARE 56 SS-Auger Elevation: 014 55 SAMPLE TYPE Intelevation: 014 56 Intelevation: 014 56 SINCALL TYPE Intelevation: 014 56 Intelevation: 014 56 SINCAL: Company: 120 min. 120 m	Proj	ect: Olds	Mountain View Subdivision				lling Inf0 ck Drillin			nment	al Ser	vices				+		le No.:8 No.:38		
Construction Bit determinant Construction	01-	n)- KANAL	Group		\rightarrow						11 GCI	1663				+				
ACKULUTYPE EXTENT E PEAGANEL [[]]SOUCH CONTROL OPTIMOS SAND SOUL OPTIMOS SOL DESCRIPTION SOL SOL SOL DESCRIPTION SOL SOL DESCRIPTION SOL SOL DESCRIPTION SOL SOL SOL DESCRIPTION SOL SOL SOL SOL SOL SOL SOL SOL					E SAN					E	2	GRA8	SAM	<u>າ</u> ເຮ	[]	_				REC
Image: Solution of the soluti	-											GRCL	л		E		NUT CO.	TTINGS	SA	٩D
0 X2:: Topsal - aprox. 150mm thick. Silly Cay (Tay) - fun, damp, sone, trace sand. 5-1 - trace sand. - trace sand. - trace sand. - silf. - trace sand.one, low plastic. 5-2 - silf. - trace sandsone, low plastic. 5-3 - trace sand.one, low plastic. 5-3 - trace sandsone, low plastic. 5-3 - trace free water, sand lense, medium gray. 5-4 - trace free water, sand lense, medium gray. 5-4 - trace free water, sand lense, medium gray. 5-4 - trace free water, sand lense, medium gray. 5-5 - trace free water, sand lense, medium gray. 5-4 - trace free water, sand lense, medium gray. 5-5 - trace free water, sand lense, medium gray. 5-5 - trace free water, sand lense, medium gray. 5-6 - moist. 5-6 - moist. 5-7 - Sill - dense, dry, medium gray. 5-6 - moist. 5-7 - moist.			SOIL	MPI F TYPF	AMPLE NO	uscs	BLOWS /150 mm	PLA	STIC	MLC.	LiQ	טוט		0 :	20	30 _	40			
0 Image: set of the set o	~	×		J.					10 1	20 30		- I		POC 1	KETPEN 60 2	1 (XPa) 240) ● 320 _		_	
 stif. - irace sandstone, low plastic. - irace sandstone, low plastic. - low to medium plastic. -	-0		Silty Clay (Till) - firm, damp, som sand, trace gravel, medium plast trace oxides, medium brown.	e lic,	5-1	TPSL			119			·····						. [SO	4] = 0.02%	
 a a second sec						G			-									•		
4 5 5 - trace free water, sand tense, medium grey. 6 5:4 7 Silt - dense, dry, medium grey. 7 Silty Ciay (Til) - silf, damp, trace gravel, medium prey. 8 - moist. 9 END OF HOLE at: a depth of 9.1 m. 25 m PVC standpips installed to a depth of 9.1 m. 25 m PVC standpips installed to a depth of 9.1 m. 25 m PVC standpips installed to a depth of 9.2 m. Water Levels: March 07, 2008 - 2.93 M April 02, 2008 - 2.95 M 10 Water Levels: March 07, 2008 - 2.93 M April 02, 2008 - 2.95 M	-2		- Irace sandstone, low plastic.		5-2			•••••									•			
5 - trace free water, sand lense, medium grey. 6 Silt - dense, dry, medium grey. 7 Silty Clay (Til) - slif, damp, trace gravel, medium plasic, trace oxides, medium grey. 8 - moist. 9 END OF HOLE at a depth of 9.1m. 25.6 10 Water Levels: March 07, 2008 - 2.95 M	-3 *		- low to medium plastic.		5-3															
7 Silt - dense, dry, medium grey. 7 Silty Clay (Til) - stiff, damp, trace gravel, medium plastic, trace oxides, medium grey. 8 - moist. 9 END OF HOLE at a depth of 9.1m. 25mm PVC standpipo installed to a depth of 9.1m with 6.1m stolled. Dry upon completion. 10 Water Levels: March 07, 2008 - 2.93 M April 02, 2008 - 2.95 M	4				5-4	CL-ML			140			······································						•		
7 gravel, medium plastic, trace oxides, medium grey. 8 - moist. 9 END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m stolled. Dry upon completion. 10 Water Levels: March 07, 2008 - 2.93 M April 02, 2008 - 2.95 M	6					мL		•••••	12.8			· · · · · · ·						-		
 8 - moist. 9 END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m slotted. Dry upon completion. 10 Water Levels: March 07, 2008 - 2.93 M April 02, 2008 - 2.95 M 	-7		gravel, medium plastic, trace oxid	des,	5-5															
25mm PVC standpipe installed to a depth of 9.1m with 6.1m slotted. Dry upon completion. Water Levels: March 07, 2008 - 2.93 M April 02, 2008 - 2.95 M	-8		- moist.		5-6															
March 07, 2008 - 2.93 M April 02, 2008 - 2.95 M	-7 -7 -8 		25mm PVC standpipe installed to depth of 9.1m with 6.1m slotted, upon completion.	ba [· · · · · ·												
		6	March 07, 2008 - 2.93 M April 02, 2008 - 2.95 M								sed By	v: Don	ninik k	(en			Com	 pleticn C	Depth: 30 f	
McIntosh Lalani Engineering Calgary, AB (403) 291-2345 Contract Real Contract Real Con	A		McIntosh Lalan Calgary, AB	i Engine	ering)				Rev	ewed	By: L	ee Ma	ırlin	-		Dolle	ed on: 2/2	25/2008	_

Proj	ect: Old:	s Mountain View Subdivisio	n				ormation:				Borehol		
				_			ng & Envin	onmenta	I Service	s		No.:3899	
	nt: MMM						S-Auger		Manu			n:1015.44	
	LE TYP		CORE				SPT SAMP				AUGER SA		 RY
BACK	FILL TY	PE BENTONITE	PEA (GRAV	ÆL T		SLOUGH		GRO		DRILL CUT	TINGS 🚺 SAND	
Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTIO	Z SAMPLE TYPE	SAMPLE NO	USCS	BLOWS /150 mm		M.C.		BLOW COU 10 20 30 POCKETPEN 80 160 24) 40]kPa) 🏶	OTHER DATA	Elevation (m)
0	Mr. N.	Topsoil - approx. 150mm thi	ck.		TPGL		10	20 30	<u>40</u>	80 160 24	320	• •	<u> </u>
-1		Sandy Silt (Till) - dense, dar gravel, fight brown.	np, trace	€-1	NLS		101						1015
-2		Silty Clay (Till) - stiff, damp, sand and gravel, medium pla trace oxides and coal, mediu brown.	astic.	6-2 6-3		5-15-7							1014-
-3				6-4		6-8-9							1013-
⊻ -4		(2	- 1	6-5	CI		14.9						1012
-5		- spoon on a rock.	X	6-6 6-7		7@4"							1011 [.]
-6		REFUSAL on a boulder at a 5.5m. 25mm PVC standpipe instelled to a depth of 5.5m v 3.0m slotted. Dry upon comp	depth of										1010-
-7		Water Levels: March 07, 2008 - 4.64 M April 02, 2008 - 3.64 M											1009-
-8													1608-
9													1007-
-7 -8 -9 -10													1006-
								Logge	d By: Don	ninik Kan	Comel	ation Depth: 18 ft	1005-
Λ		McIntosh La Calgary, A8	lani Engineer	ing					wed By: Lon			on: 2/25/2008	
		(403) 291-23	46				ł			epth: 3.64 m	Page 1		







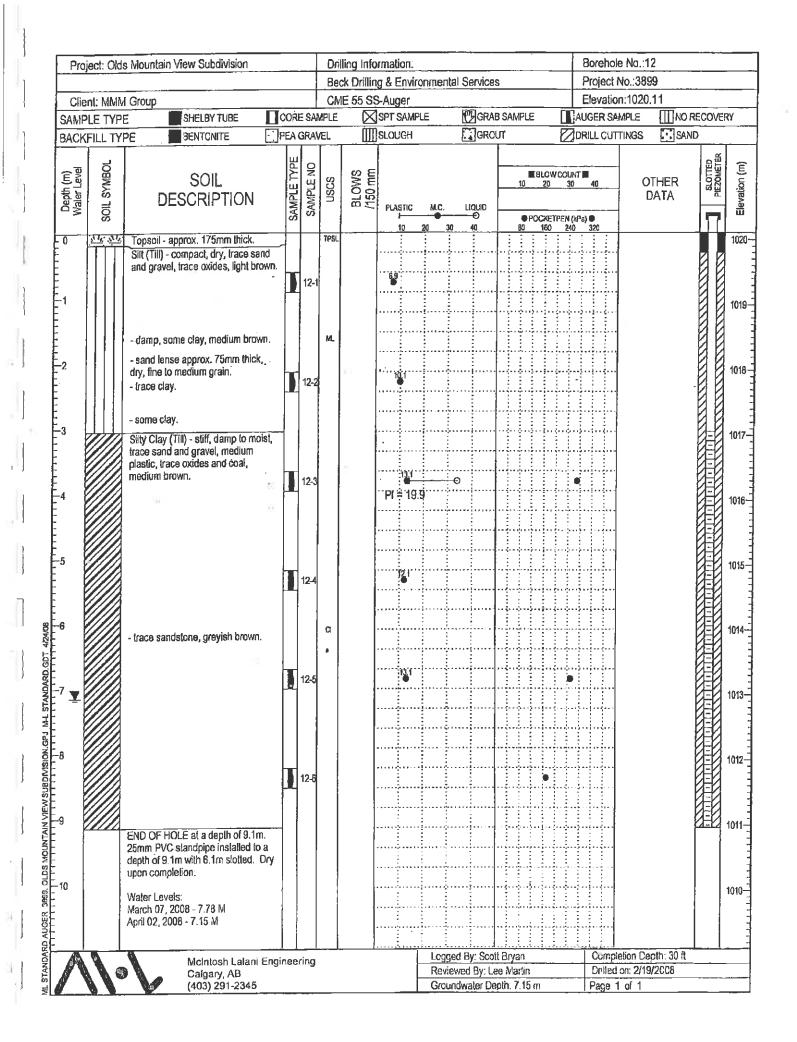


Pro	ject: Old	s Mountain	View Subdivision					ormation:								e No.:11			
								ng & Envir	onmen	al Servic	8 8				-	No.:3899			
	ent: MMN							S-Auger	1 10	GR		201 F				n:1018.2			
	LETYP		SHELBY TUBE		RE SA			SPT SAMP		GR		NPLE		AUG					RY
BACK	FILL TY	PE (BENTONITE	PE/	GRA		<u>ш</u>	SLOUGH		L-B GK				DRIL	LCUS	IINGS	SAN		<u> </u>
Depth (m) Water Level	SOIL SYMBOL	D	SOIL ESCRIPTION	CANNUT TUTA	SAMPLE NO	USCS	BLOWS /150 mm		M.C.		1	10 @P(CKETPE	30 4 N (XPa) 4	10		HER ATA	BLOTTED PIEZOMETER	Elevation (In)
		Silt (Till) - and grave Silty Clay sand and trace oxid brown. - medium Silt (Till) - sand and trace oxid brown.	compact, damp, trace siltstone, medium grey. IOLE at a depth of 9.1m C standpipe installed to .1m with 6.1m slotted. I pletion.		11-2 11-2 11-3 11-4 11-5 11-5 11-7 11-8	Cł	3-6-8 2-7-9 - 1-7-8 2-3-7 3-4-7			-									1018- 1016- 1015- 1014- 1011- 1012- 1011- 1010- 1009-
		March 07,	2008 - 3.64 M 008 - 3.76 M																1008-
		2	McIntosh Lalani	Engine	erina					ed By: Sc						tion Depl		·	
	A G		Calgary, AB							ewed By:						on: 2/15/2	8008		
0	0 0		(403) 291-2345						Grou	indwater (Depth: 3	3.64 r	n	P	age 1	of 1			

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Γ.



Pro	ject: Old	s Mountain View Subdivision		1			rmation:		- Contoo		Borehole	e No.:13 No.:3899		
	ent: MMM	l Group		-		E 55 SS	g & Enviro	nmenta	al Services	5		n:1016.90		
			CORE	E SAN			SPT SAMPI	Ē	GRA	B SAMFLE	AUGER SA		ECOVE	RY
	FILL TY						SLOUGH	- · -	GRCI	UT 🛛	DRILL CUT)	
Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO	USCS	BLOWS /150 mm		M.C.		POCKETPEN) 40 (kPa) ●	other Data		Elevation (m)
-0	3 18 N 14	Topsoil - approx. 150mm thick.			TPSL		10	<u>20 30</u> : :	40	80 160 24	0 320			ļ
		Silt (Till) - compact, dry, trace sand and gravel, trace oxides, medium brown.	I	13-1	ML		10.8					[SO ₄] = 0.147%		1016-
2		Silly Clay (Till) - stiff, damp to moist trace sand and gravel, medium plastic, trace oxides and coal, medium brown.	X	13-2		4-5-8	87							1015-
-3		-		13-3						· · · · · · · · · · · · · · · · · · ·				1014
- - - - - - - - - - - - - - - - - - -		- đark brown.		13-4 13-5		4-8-10	-							1013
5		- trace siltstone, no gravel, medium grey.		13-6 13-7	СІ	5-8-10								1012
1 4/14/08 09		 trace gravel, greyish brown. 	X	13-8		4-8-10								1011-
		• nace grave, greyen crown.	T	13-9										1010
		- trace sandstone, trace free water i spoon, medium grey.		13-10 13-11		5-5-8								1009
		END OF HOLE at a depth of 9.1m.												1008-
		25mm PVC standpipe installed to a depth of 9.1m with 6.1m slotled. Dry upon completion. Water Levels:	y			Ĩ						l		1007
		March 07, 2008 - 7.09 M April 02, 2008 - 5.82 M					·····							1006
		McIntosh Lalani Er	ngineei	ring					ed By: Scol			etion Depth: 30 ft on: 2/20/2008		
		Calgary, AB (403) 291-2345					· [wed By: Le	epth: 5.82 m	Page 1			

	Pro	oject: Old	s Mountain View Subdivision					irmation:			Borehole No.		
								g & Environment	al Services	<u>}</u>	Project No.:3		
		ent: MMN					<u>AE 55 SS</u>				Elevation:101		
		PLE TYP				MPLE		SPT SAMPLE			AUGER SAMPLE		:OVE
	BACK	FILL TY	PE BENTONITE	PE/	GRA	VEL		SLOUGH	GROU		DRILL CUTTINGS	SAND	
	Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMDI E TVDE	SAMPLE NO	ISCS	BLOWS /150 mm	PLASTIC M.C.		BLOW CO 10 20		OTHER DATA	SLOTTED PIEZOMETER
	->	l S		5	5 3			10 20 30	LIQUID ——€) 40	POCKETPEN 80 160 2	N (kPa) ● 240 320	Í	7
Ì	- 0	34.34	Topsoil - approx. 125mm thick.		-	TPSL		10 20 30		<u>80 160 2</u>	<u>40 320</u>		H
	-		Silt (Till) - compact, dry, some sa trace gravel, trace oxides, light brown.		14-1	ML							
			Silty Clay (Till) - stiff, moist, trace sand and gravel, medium plastic trace oxides and coal, medium	ə ;									
	-2		brown.		14-2			12.8			•		
<u></u>	-3			62									
والرغابات فالمحقولة	-4				14-3			V		•	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
	-5												
				I	14-4	CI		130					
.GDT 4/14/08	6		- trace siltstone, međium grey.										
1 STANDARD.GDT	7				14-5								
N Cdb Noisin	8 ₹												
N VIEW SUBDI	g				14-6								
THE REPORT OF STREET AND A ST			END OF HOLE at a depth of 9.1m 25mm PVC standpipe installed to depth of 9.1m with 6.1m slotted. (upon completion.	a			•						
GER 3899.	10		Water Levels: March 07, 2008 - Dry at 8.74m April 02, 2008 - 8.0m				•						
ANDARD AU													

	Pro	ject: Old	's Mountain View Subdivision				ormation:				1	e No.: 15	
		ent: MMA	1 Crown			ME 55 S	ng & Envir	onmenta	I Service	S	<u> </u>	No.:3899 n:1014.29	
:		PLE TYP		CORES			SPT SAME	νE	13 GRA	3 SAMPLE	AUGER SA		ECOVERY
		FILL TY		PEA GR			SLCUGH		GRO				
	Depth (m)	SYMBOL	SOIL		USCS	05				BLOWCOL		OTHER	PIEZOMETER PIEZOMETER Elevation (m)
		SOIL SOIL	DESCRIPTION	SAMP			PLASTIC 10	M.C. 20 30	LIQUID 0 40 :	● POCKETPEN 80 160 24		DATA	
			Silt (Till) - compact, dry, some sar trace gravel, trace oxides, light brown.	nd,			25					•	1014
	-2		- spoon on a rock. Silly Clay (Till) - stiff, damp to moi	15	+2	bouncing	8,6						1013
	-3		 Sity Citay (Thi) - Suit, damp to more trace sand and gravel, medium plastic, trace oxides and coal, medium brown. very stiff, trace precipitates in 	st, 15	-	4-7-11						2	1012
	-4		spoon.	15			∏PI ≆ 23	1			•	[SO₄] = 1.070%	1011
	-5		- trace sandstone, medium grey.	15		4-8-11	120						1010
DT 4/24/08	-6		- poor sample recovery.	15	a	5-8-9							1008-
U M-L STANDARD.GI	-7			15		67.40							1007-
IEW SUBDIVISION.G	-8			15-		5-7-10							1006-
STANDARD AUGER 3899 OLDS MOUNTAIN VIEW SUBDIVISION GPJ M-L STANDARD.GDT	-9		END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m statled. E upon completion. Water Levels: March 07, 2008 - Dry to 9.07m April 02, 2009 - Dry to 9.07m	a									1005-
AL STANDARD AUG			April 02, 2008 - Dry to 9.03m McIntosh Lalani E Gaigary, AB (403) 291-2345	Engineerin	9			Review	d By: Scot wed By: Le dwater De	e Martin		etion Depth: 30 ft cn: 2/20/2008 of 1	

Project: Olds Mountain View Subdivision			lling Info					e No.:16
Client: MMM Group			E 55 SS	3 & Environment: Auger	al Service	5		No.:3899 n:1014.34
SAMPLE TYPE SHELBY TUBE	CORE SA			SPT SAMPLE	GRA	B SAMPLE	AUGER SA	
BACKFILL TYPE	PEA GRA	VEL		SLOUGH	GRO	υτ	DRILL CUT	
	SAMPLE TYPE SAMPLE NO	USCS	BLOWS /150 mm	plaștic M.C.	LIQUID	10 20	COUNT III 30 40	OTHER DATA
0 A Topsoil - approx. 305mm thick.				10 20 30	Ð	60 150	IPEN (kPa) ● 240 320	
Silt (Till) - compact, damp, trace sand and gravel, trace oxides and coal, medium brown. - (race clay.	16-1	TPSL ML						
Silty Clay (Till) - stiff, damp to mois trace sand and gravel, low plastic, trace oxides and coal, medium brown, - medium plastic.	st, 16-2	CL-NL		112				
¥	16-3			1222				
- dark brown.	16-4	сі		15				
- moist, dark grey.	18.5							
	16-5		••		<u>-</u>			
END OF HOLE at a depth of 9.1m.	16-6		••					
25mm PVC standpipe installed to a depth of 9.1m with 6.1m slotted. Dr upon completion. Water Levels:	y							

rių	ject: Old	s Mountain View Subdivision				ormation: 19 & Envin	onmont	d Comitor			ole No.:1		
Clie	ent: MMM	1 Group	-			S-Auger	vinicili	AL ORLAICE			t No.:389		
	PLE TYPI		CORE S			SPT SAMP		68121000	BSAMPLE		on:1015.		
	FILL TYP									AUGER		MO RE	COVERY
DACK	1116 Y		PEA GRA		<u>Ш(</u>	SLOUGH		GRC	UT		TTINGS	SAND	
Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE SAMPLE TYPE	USCS	BLOWS /150 mm	PLASTIC	N.C.	Liquid 	10 20	30 40		'HER Ata	SLOTTED PIEZOMETER
-	\$4:84	T . 1		TPSL		10	20 30	40	POCKETP 80 160	EN (MPa) 240 320			17 '
0		Topsoil - approx. 125mm thick. Sill (Till) - compact, damp, trac sand, clay and gravel, trace ox medium brown. - some clay.	3								•		10
		Silty Clay (Till) - very stiff, damp moist, trace sand and gravel, medium plastic, trace oxides an coal, medium brown.	<u> </u>		9-11-14		1				120		10
		01	17-4		2-8-9	12.9					И		101
¥			17-5			13.2					(I)		101
		- dark greyish brown.	× 17-6		5-14-12	•			•				101
			17-8		3-10-14								1010
		- trace sandstone, medium grey.	17-10		4-7-9								1003
		sansoono, mouun groy.	1 7-1		-			····					1007-
	2 d u	END OF HOLE at a depth of 9.1r 25mm PVC standpipe installed to depth of 9.1m with 6.1m slotted. upon completion.	a		•••								1006
	1	Nater Levels: Aarch 07, 2008 - 4.44 M April 02, 2008 - 3.92 M											1005
A'		McIntosh Lalani	Engineering					By: Scott			ion Depth:		<u> </u>
/ 🐃		Calgary, AB (403) 291-2345				L		ed By: Lee	Martin h: 3.92 m		n: 2/21/200		

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Proj	ect: Olds	s Mouritain View Subdivision				illing Info			0			e No.:18		
					-		g & Enviro	onmenta	Service	<u>es</u>	+ ·· ·	<u>No.:3899</u>		
	nt: MMM			RE SA	_	VIE 55 SS	SPT SAMP	F	M CR4	AB SAMPLE	AUGER SAI		FCOVE	RY
							SLOUGH						_	
BACKI	FILL TYI	PE				<u></u>			<u></u>		JUNICE OUN		1	Τ
Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMDI 5 TVD5	SAMPLE NO	USCS	BLOWS /150 mm		M.C.		POCKETPE/	30 40	other Data	PIEZOMETER	Elevation (m)
- 0	<u>x 4. x 1.</u>	Topsoil - approx. 305mm thick.	-+-		TPSL		10	<u>20 30</u>	<u>40</u> :	80 160 2	40 320			
		Silt - compact, damp, trace sand, dark grey.		18-1			11.9							1010
-1		Silt (Till) - compact, damp, trace sand and gravel, trace oxides, medium brown.		-	ML									
		Silly Clay (Till) - stiff, moist, trace	<											1009-
		sand and gravel, medium plastic, trace oxides and coal, medium brown.		18-2			144 PI ≢ 25.	5	- 0			•		4000
-3		ω.					-							1008-
		£	2	18-3		•	13.6				•			1007-
-4		X			α									
-5							12.8							1006-
		- greyish brown.		18-4			•							1005-
-6														
-7	(///	Bedrock (Sandstone) - very strong damp, medium grey. REFUSAL in bedrock at a depth o	, /⊢	18-5	BE									1004
		6.8m. 25mm PVC standpipe installed to a depth of 6.8m with 4.6m slotted. Dry upon completio	n.						••••					1003-
-7 -8 -9		Water Levels: March 07, 2008 - 2.51 M April 02, 2008 - 2.65 M								-				1000
-9														1002
														1001
-10														
		62						0000	1 84. 50	olt Bryan	Como	ielion Depth; 22.3 f	 t	1000
A		McIntosh Lalani	Engine	ering			ŀ			Lee Martin		en: 2/21/2008	·	
N	6 V 6	Calgary, AB (403) 291-2345					ļ			lepth: 2.51 m	Page			

Pro	oject: Ol	ds Mountair	View Subdivision			-	rilling Inf eck Drilli		-	ome	ofal	Senio				_			ble No.: t No.:38			
Clie	ent: MM	M Group					VE 55 S			1010	ILCII V	Q GI VIO	69				_		ion:102(_	_ .	
	PLETY		SHELBY TUBE	Tco	ORE SA			SPT SA	_	F	-	GR	AR :	SAMP	7 F	П			AMPLE		9500	
	FILL TY		BENTONITE	_	A GRA			SLOUG				GRI	_						TTINGS			VERT
Depth (m) Water Level	Τ.		SOIL		SAMPLE TYPE SAMPLE NO	1	BLOWS 150 mm				(,)THER	SLOTTED	ZOMETER
Wate	S TICS	D	ESCRIPTION		SAMPL	SN	BLC	PLAST		M.C.	30	1.10(UID 			POCK	ETPEN	l (kPa) 40	320		DATA	~ ~	
0		Silt (Till) - trace grav brown.	approx. 150mm thick. compact, dry, some sau rel, trace oxides, light ace send and clay, rowa.	nd,	19-1	ML	6-8-11		15.2									320				
2		Silty Sand medium g	- compact, damp, fine f rain, medium brown.	•	19-2		0-0-11	7,2														
		trace sand			(19-4 19-5		-11-14@4												98 82			
		- dark brow	nish grey.		19-6		3-9-16						· · ·				•					111111111111111111111111111111111111111
¥		- spoon on	a rock, medium grey.		19-8	CI												****				1
					19-9 19-10		2-4-8															10
		25mm PVC depth of 9.1 upon compl Water Level	s: 008 - 8.01 M	ry																	K-K	10 101
			McIntosh Lalani El Calgary, AB (403) 291-2345	nginee	tL ering		1.	<u></u>		Revi	ewed	: ly: Scol I By: Le aler De	:e 1	Aartin		<u></u>	1		etion Dep on: 2/15/			

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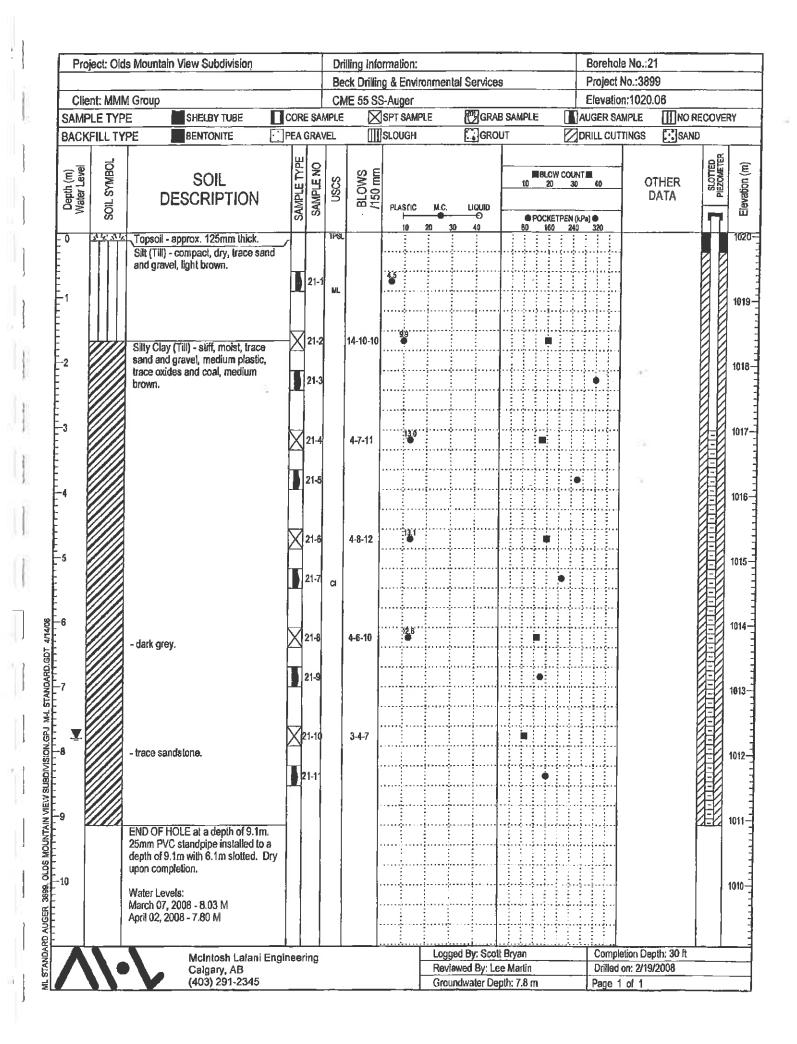
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Proj	ect: Old	s Mountain View Subdivision		-	-		ormation: Ig & Environme	ntal Services		Borehole Project N	··- ·	
Clie	nt: MMM	/ Group		+			S-Auger				1: 1018.7 5	
	LETYP		COR	E SAN	-		SPT SAMPLE			AUGER SAI		RECOVERY
	FILL TY		PEA	GRAV	/EL		SLOUGH	GRCI	JT Z	DRILL CUT	INGS 💽 SAN	D
Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO	nscs	BLOWS /150 mm	PLASTIC M.C	LIQUID 30 40	BLOWCOU 10 20 3 POCKETPEN B0 160 24	0 <u>40</u> (kPa)●	OTHER DATA	PIEZOMETER
0	<u> A 4 A 14</u>	Topsoil - approx. 225mm thick.			TPSL							
1		Sandy Silt (Till) - compact, dry, tra gravel and oxides, light brown.	Ce	20-1	MLS		3					10
2		Siity Clay (Till) - sliff, moist, trace sand and gravel, medium plastic, trace oxides and coal, medium brown.		20-2			122		· · · · · · · · · · · · · · · · · · ·		[SO4] = 0.017%	10
I		- dark brownish grey. - medium grey.	I	20-3					•			10
.			1	20-4	a							10
			J	20-5								10
				20-6								101
D		END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m slotted. D upon completion. Water Levels: March 07, 2008 - 5.57 M April 02, 2008 - 4.93 M										100
		- year and a constant of the second										100
A		McIntosh Lalani E Calgary, AB	inginee	ring	11			gged By: Scot viewed By: Le			elion Depth: 30 ft on: 2/15/2008	

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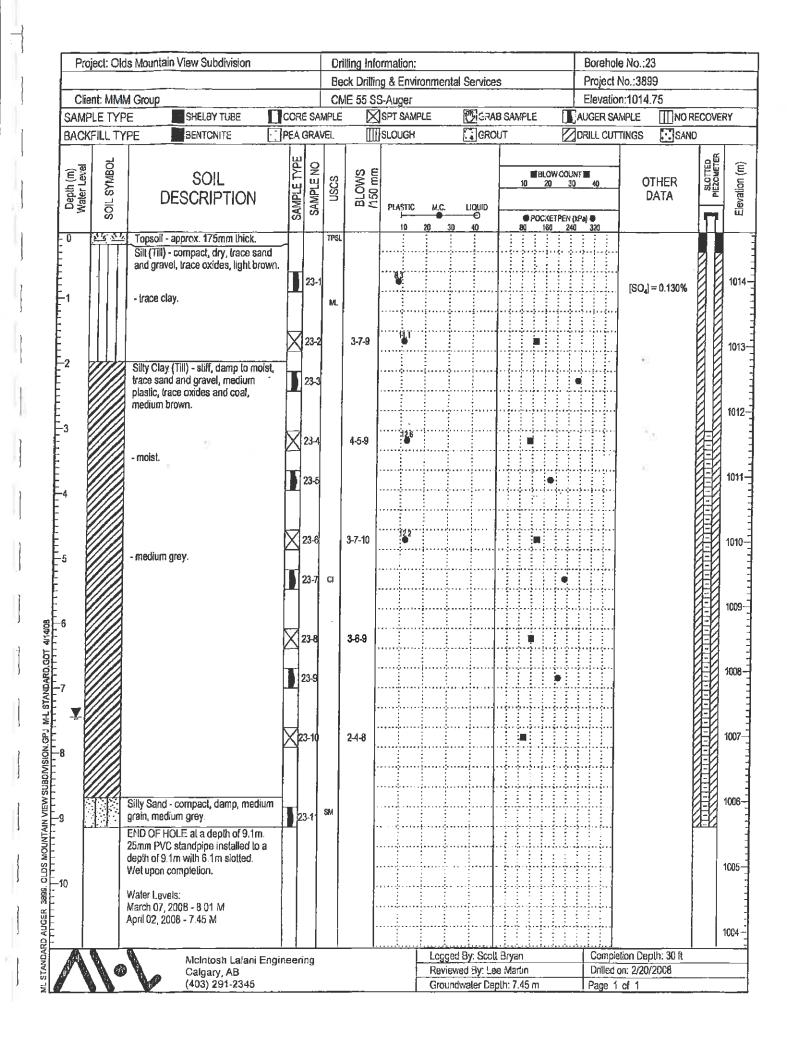


	oject: Old	s Mountain View Subdivision					rmation:					e No.:22		
		1 Carrier		_			ig & Enviro	onmenta	Service	<u> </u>		No.:3899		
	ent: MMN PLE TYP		COF			<u>AE 55 SS</u>	SPT SAMP		Sel com	B SAMPLE	L	n:1017.48		
							SLOUGH		GRO		AUGER SA			ERY
BACK	(FILL TY			GRAN		<u>т ши</u>	ISLOUGH		GRU		DRILL CUT		ND	
Depth (m)	SOIL SYMBOL	SOIL	SAMPI F TYPF	SAMPLE NO	nscs	BLOWS /150 mm	PLASTIC	M.G. 20 30		BLOW COU 10 23 3 POCKETPEN 80 16C 24	0 40 (kPa) •	OTHER DATA		Elevation (m)
0	31.31	Topsoil - approx. 125mm thick.		1	TPSL						320			
-1		Silt (Till) - compact, dry, trace sar and gravel, trace oxides, light bro	nd wn,	22-1	ML		*							101
-2		Silty Clay (Till) - stiff, damp, trace sand and gravel, medium plastic, trace oxides and coal, medium brown.		22-2		×	•							1016
-3														1014
-4		- moisl.		22-3			127							1013
-5		- damp to moist, medium grey.	J	22-4	CI		13.8							1012
7			J	22-5										1011 1011
8		- some sand, lense throughout. - trace sillstone, light grey.		22-6										1009
9		END OF HOLE at a depth of 9.1m 25mm PVC standpipe installed to depth of 9.1m with 6.1m slotted. If upon completion.	a											1008-
•		March 07, 2008 - Dry to 8.78m April 02, 2008 - Dry to 8.79m McIntosh Lalani i	Enginee	ening					d By: Scol		Comple	tion Depth: 30 ft		1007-
		Calgary, AB (403) 291-2345		5			ļ		ved By: Le dwater De			m: 2/19/2008		

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C S C PARTC LC LC LC Description 0 CA AC Description	Projec	t: Olds Mountain View Subdivision	תל		rilling Inform				Borehole		
SAMPLE TYPE INIT OF THE INFORMATION INFORMATIONI	Client	MMM Group					al Services	·	- · · · · · · · · · · · · · · · · · · ·		
BACKFILL TYPE BENTONTE PER GRAVEL BISLOUGH All GROUT Distance Image: Solid operation of the solid operation of the solid operation operation operation operation. Solid operation operation operation operation operation operation operation operation. Image: Solid operation operation operation operation operation operation operation operation operation operation. Image: Solid operation operation operation operation operation operation operation operation operation. Image: Solid operation operation operation operation operation operation operation operation operation. Image: Solid operation operation operation operation operation operation operation operation operation. Image: Solid operation operation. Image: Solid operation operatioperatioperation operation operatioperation operation operation op		· · · · · · · · · · · · · · · · · · ·					M cour				070
Solution Solut											
Image: Solution of the second seco	DRUKII			AVEL				<u>" č</u>			_
0 25 26 Topsol - soprox. 200mm thick. 0 25 24 Topsol - soprox. 200mm thick. multiple compact dam, trace cides, medium brown. -1 Sil (711) - stift, damp to molst, trace cides and and gravel, medium brown. 24-1 multiple compact dam, medium prov. -2 Sil (711) - stift, damp to molst, trace cides and coal, medium brown. 24-2 4 1 <td>Depth (m) Water Level</td> <td>SOIL DESCRIPTIO</td> <td>AMPLE TYPE</td> <td>USCS</td> <td>BLOWS /150 mm</td> <td>PLASTIC M.C.</td> <td>Liquid</td> <td></td> <td></td> <td></td> <td>at Officen</td>	Depth (m) Water Level	SOIL DESCRIPTIO	AMPLE TYPE	USCS	BLOWS /150 mm	PLASTIC M.C.	Liquid				at Officen
1 Sill (TII) - compact damp, trace oxides, medium brown. - 2 Silly Clay (TII) - stift, damp to molet, medium brown. - 2 Silly Clay (TII) - stift, damp to molet, medium brown. - 3 Silly Clay (TII) - stift, damp to molet, medium brown. - 4 Silly Clay (TII) - stift, damp to molet, medium brown. - 4 - 4 ark brown. - 4 ark brown. 24-3 - 6 - moist, medium grey. 5 - moist, medium grey. 6 - trace sillsione. 24-6 - 1 mole sillsione. 24-7 - trace sillsione. 24-8 - 1 mole sillsione. 24-6 - 1 mole sillsione. 24-7 - 1 mole sillsione. 24-8 - 1 mole sillsione. 24-9 - 1 mole sillsione. 24-6 - 1 mole sillsione. 10 Waler Levels;						10 20 30					
- some clay some clay some clay a Silly Clay (Till) - still, damp to moist, the as and and gravel, medium plaste, three oxides and cost, medium gravel, medium gray a some clay a dark brown		Silt (Till) - compact, damp, t clay, sand and gravel, trace	oxides,			8,1					
Sily Clay (Til) - stift, damp to molst, trace sand and gravel, medium plastic, frace oxides and cool, medium brown. - dark brown. - trace sillstone. - trace sill trace sillstone. - trace si		- some clay.									
Image: serie and dr gravel, medium proven. - dauk brown. - moist, medium grey. - moist, medium grey. - urace siltstone. - urace siltstone. <td>-2</td> <td></td>	-2										
 - moist, medium grey. - moist, medium grey. - trace siltstone. - trace siltstone. 24-6 2		trace sand and gravel, media plastic, trace oxides and coa	um 📕 🖺	2		•					
-4 		- dark brown.				13.4					
-5 -6 -6 -6 -6 -6 -7 -6 -7 -6 -7 -7 -7 - trace sillstone. 24.5			24-	3		•					
-6 -6 - trace siltsione, - trace siltsione,	5	- moist, medium grey.			• • •					12	
-7 -8 -9 END OF HOLE at a depth of 9.1m. 24.6 24.6 END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m stotled. Dry upon completion. Water Levels:			24-			13.6		•			
-7 -8 -9 END OF HOLE at a depth of 9.1m. 24.6 24.6 END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m stotled. Dry upon completion. Water Levels:	-6										
-9 END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m slotted. Dry upon completion. -10 Water Levels:	-7	- trace siltstone.	3 24-5					•			
-9 END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m slotted. Dry upon completion. -10 Water Levels:											
-10 25mm PVC standpipe installed to a depth of 9.1m with 6.1m stotted. Dry upon completion.			24-6		••••						
-10 Water Levels:	-9	25mm PVC standpipe installed depth of 9.1m with 6.1m slotte	itos								
April 02, 2008 - 5.28 M	-10	Water Levels: March 07, 2008 - 7.80 M									
McIntosh Latani Engineering Calgary, AB McIntosh Latani Engineering Calgary, AB Completion Depth: 30 ft Reviewed By: Lee Martin Drilled on: 2/20/2008		McIntosh Lata Catgary, AB	ni Engineering								·

		Dject: Uid	s Mountain View Subdivision		-		lling Inf	 					Boreho				
	Clie	ent: MMN	/ Group						nmenta	I Service	5		Project				
				COR			IE 55 S	ger Sampl		- Million -	0.011/01 -		Elevatio				
		FILL TY		PEA				_	.E.		B SAMPLE	_	AUGER SA		Пио		ER
	DACK		C DENIONITE		GRAV		<u>, III</u>	UGH		GRO	JUT		DRILL CUT	TINGS	SAN	D	_
5	Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPF	SAMPLE NO	USCS	BLOWS /150 mm	ISTIC	M.C.	LIQUID	BLO1 10 20 POCKE	30	40		THER DATA	SLOTTED PIEZOWETER	L'ILLANNE LEV
	- 0	<u> 14. 11.</u>	Topsoil - approx. 225mm thick.		┝╴┨	TPSI		 10 2	10 <u>30</u>		POCKE <u>80 160</u>	240	320			-11[
DS MOUNTAIN VIEW SUBDIVISION.GPJ M-L STANDARD.GDT 4/14/08	-1		Sill (Till) - compact, damp, some clay, trace sand and gravel, trace oxides, medium brown. - trace clay, light brown. Silty Clay (Till) - stiff, damp to mol trace sand and gravel, medium plastic, trace oxides and coal, medium brown. - dark brown. - dark grey.		25-7 25-8 25-9 5-10	4	3-7-8 3-6-10 -10-10 4-7-8										1 10 100 100
STANDARD AUGER 3899. OLI		M	pon completion. /ater Leveis: arch 07, 2008 - 6,83 M pril 02, 2008 - 4,14 M														100
NE	Λ		McIntosh Lalani En	gineerin	ıg					By: Scott E			Completi				
5			Calgary, AB (403) 291-2345							d By: Lee	Martin h: 4.14 m		Drilled or Page 1 c		008		

	Pro	ject: Old	s Mountain View Subdivision					ormation: Ig & Enviro	nmont	al Senice		1	e No.:26 No.:3899		
	Clis	ent: MMN	Group					S-Auger		0019100		<u> </u>	n:1014.52		
		PLE TYP		COR	E SAI			SPT SAMPI	.E			AUGER SA			RY
	L	FILL TY		PEA	GRA	VEL		SLOUGH		GRO	ur 🛛	DRILL CUT	TINGSSAN	D	
	Depth (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO	uscs	BLOWS /150 mm	}	M.C.		POCKETPEN	10 40	other Data	PIEZOMETER	Elevation (m)
	- 0	51 6- 54 C	Topsoil - approx. 100mm thick.		-	TPSL		<u>10</u>	<u>20 30</u>	<u>) 40</u>	80 160 2	40 320		╌┧┟╌╏╸	
	1		Sandy Silt - dense, damp, frace gravel and oxides, light brown.	_ 	26-1	MLS		7					[SO4] = 0.02%		1014-
			Silly Clay (Till) - stiff, damp, trace sand and gravel, medium plastic, trace oxides and coal, medium												1013-
1	-2		trace oxides and coal, medium brown.	Ī	26-2			110			•				1012-
	-3		2 62		26-3										1011-
	-4		77(1010-
	-5			J	26-4	a		123							1009-
D.GDT 4/14/08	-6		- graval iense.												1008
PJ M-L STANDAR	-7		- medíum grey.		26-5										1007-
OLDS MOUNTAIN VIEW SUBDIVISION SPJ M-L STANDARD SDT	-8			T	26-6										1006
LDS MOUNTAIN VI	-9		END OF HOLE at a depth of 9.1m 25mm PVC standpipe installed to depth of 9.1m with 6.1m slotted. If upon completion.	a										<u>8-8</u>	1005
NDARD AUGER 3699. O	-10		Water Levels: March 07, 2008 - Dry to 9.03m April 02, 2008 - Dry to 9.02m												1004
INDARI	A		McIntosh Lalani Calgary, AB	Enginee	ring	1				ed By: Don swed By: L			elion Depth: 30 ft on: 2/25/2008	<u> </u>	
11 S.1			(403) 291-2345					-		ndwater De		Page			

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FIU	ect: Old:	s Mountain View Subdivision					ormation:				+	e No.:27	· · · · ·
Clier	nt: MMM	Group					ng & ⊑nvi S-Auger	onmen	tal Service	5	-	No.:3899	
	LE TYPE			RE SA			S-Auger		(C) CDA	B SAMPLE		n:1010.62	
	FILL TY						SLOUGH				AUGER SA		RECOVER
		E BENIONIE	PE/	I GRA			ISLOUGH		GRO		DRILL CUT	TINGS 💽 SA	
Depth (m) Water Level	SOIL SYMBOL	SOIL DESCRIPTION	SAMPIE TVDE	SAMPLE NO	USCS	BLOWS /150 mm		MLC.		POCKETPEN	1040 (kPa) ●	OTHER DATA	SLOTTED PIEZOMETER
0	<u> 14: 51.</u>	Topsoil - approx. 150mm thick.			TPSL		10	20 30	0 40	80 150 24	0 320		
		Silty Clay (Till) - very stiff, damp, trace sand and gravel, low plastic trace oxides and coal, medium brown. - medium plastic. - sandstone cobble. Silt - compact, damp, trace sand, olive brown. Silty Clay (Till) - hard, damp, trace sand and gravel, medium plastic, trace oxides and coal, medium brown. Silty Clay (Till) - hard, damp, trace sand and gravel, medium plastic, trace oxides and coal, medium brown. Silty Clay (Till) - hard, damp, trace sand and gravel, medium plastic, trace oxides and coal, medium brown. Sedrock (Sandstone) - very strong, try, light brown. Silty Clay (Sandstone) - very strong, try, light brown.		27-1 27-2 27-3 27-4 27-5 27-6 27-7 27-8 27-7 27-8 27-9 27-10 27-11	CL-ME CI ML CI	7-10-13 8-10-13 12-13-18 7-11-19							
	N	Vater Levels: Aarch 07, 2008 - 3.61 M pril 02, 2008 - 3.77 M							· · · · · · · · · · · · · · · · · · ·				10
A		Molatach i alerti Er	dincer	<u> </u>			<u> </u>	Looner	d By: Scolt	Rrvan	Completi	on Depth: 27 ft	
		McIntosh Lalani Er Calgary, AB	igineer	ing			F		ved By: Scott			on Depth: 27 It n: 2/21/2008	
		(403) 291-2345					F		waler Dep		Page 1		

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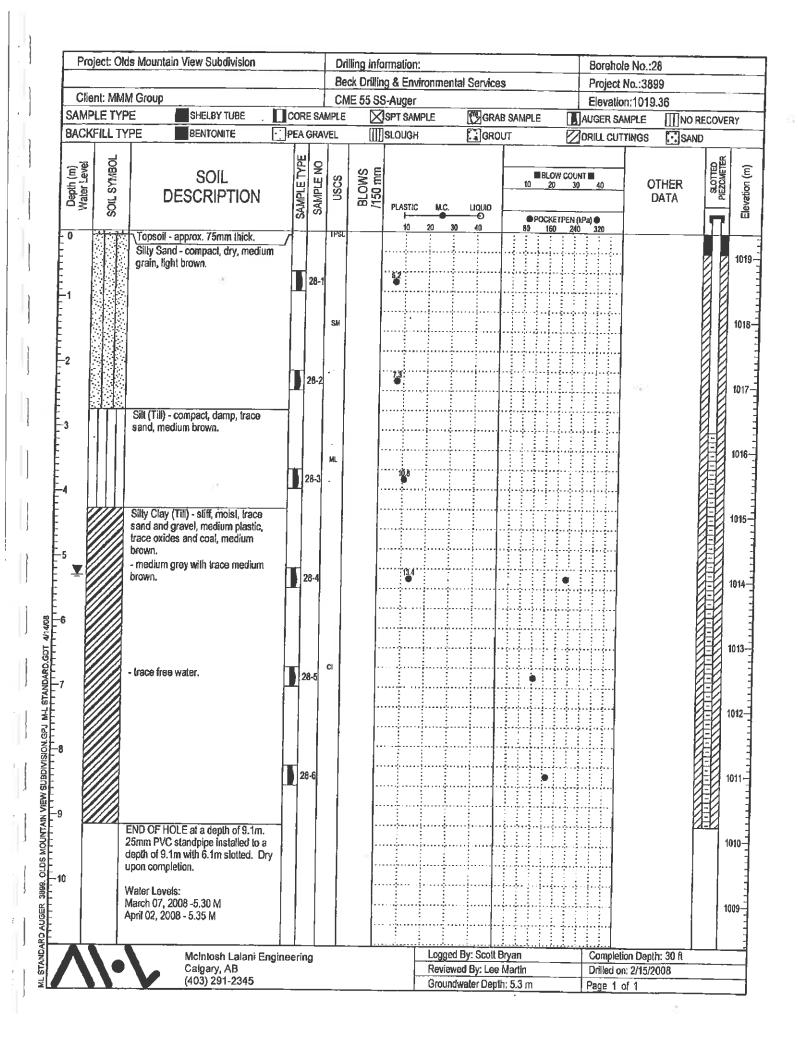
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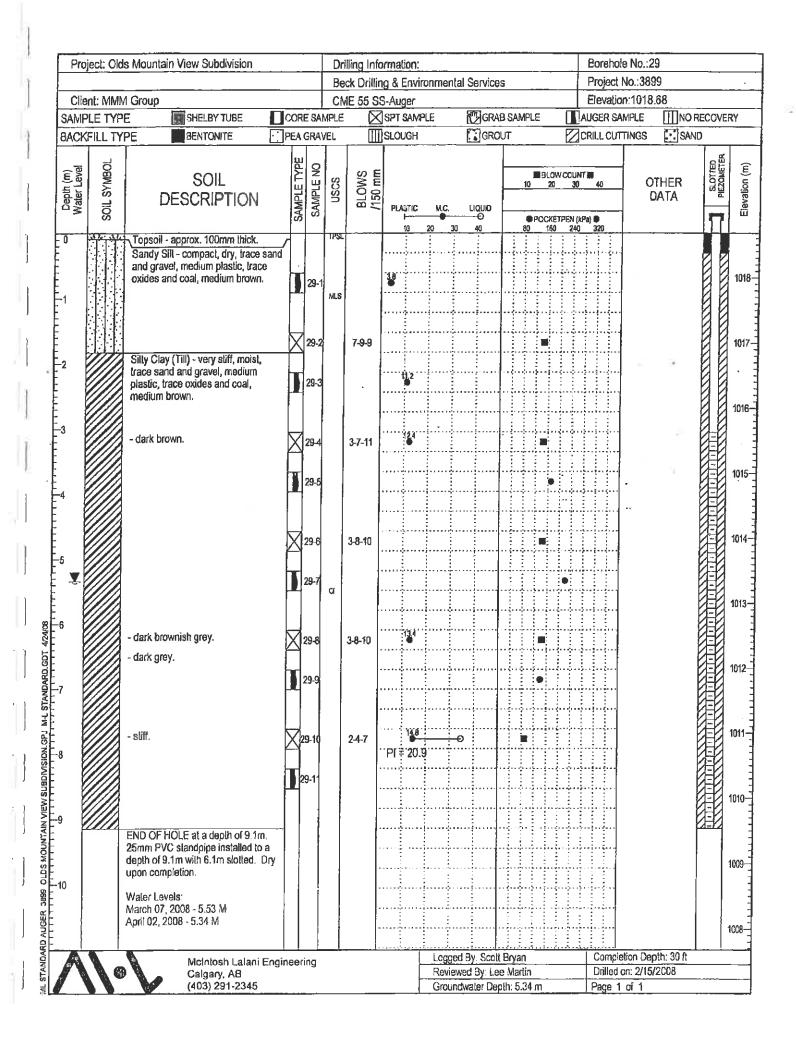
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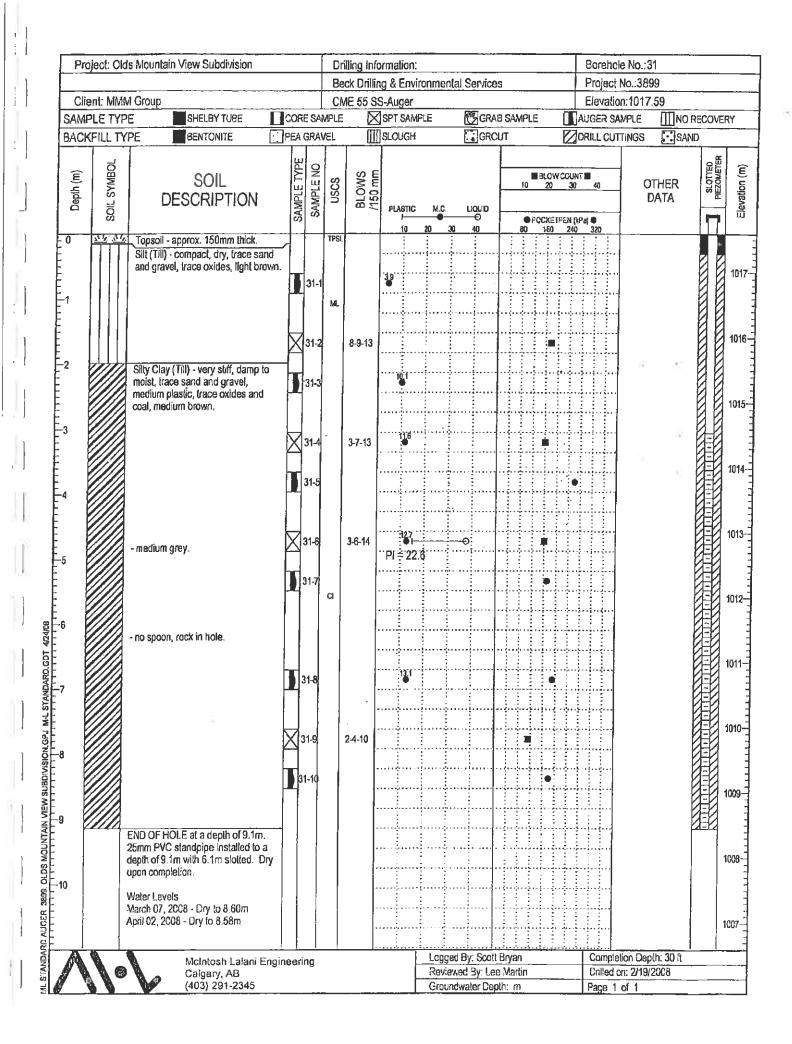
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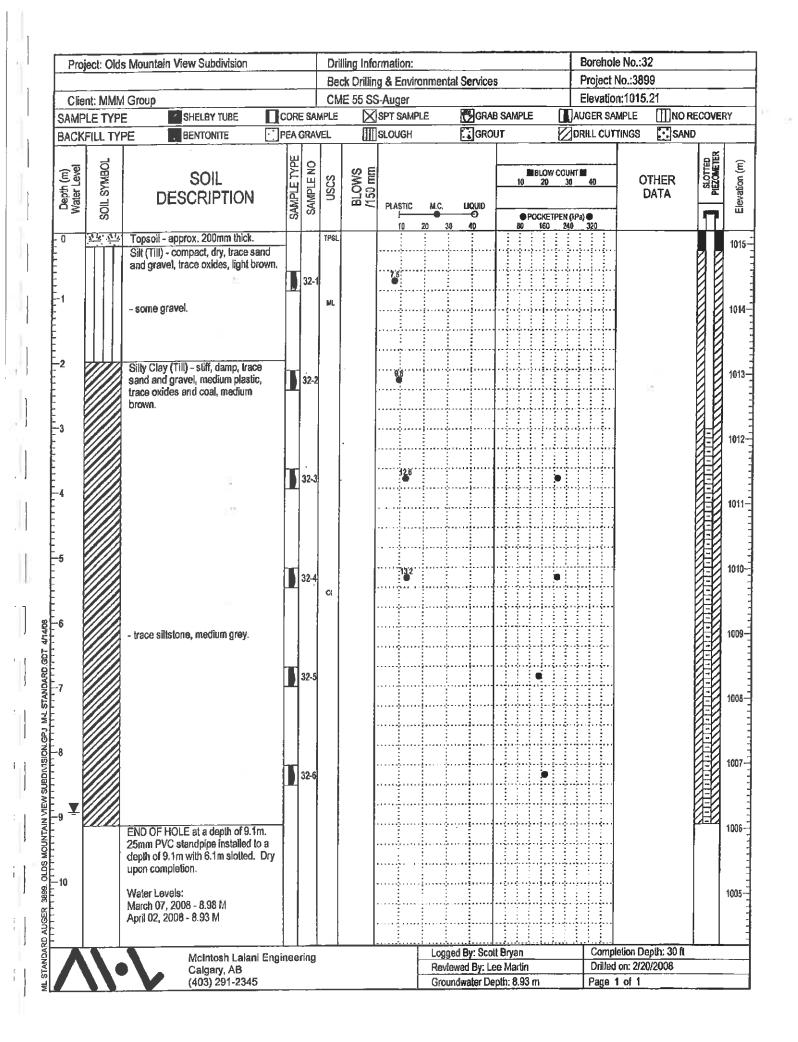


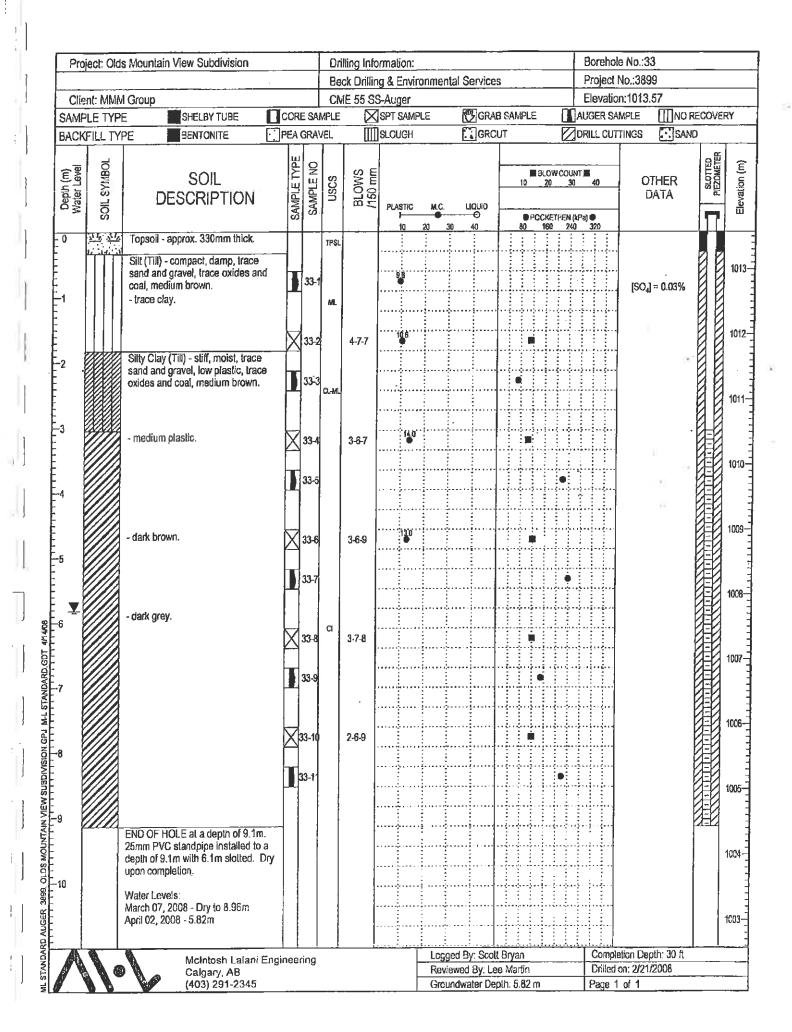


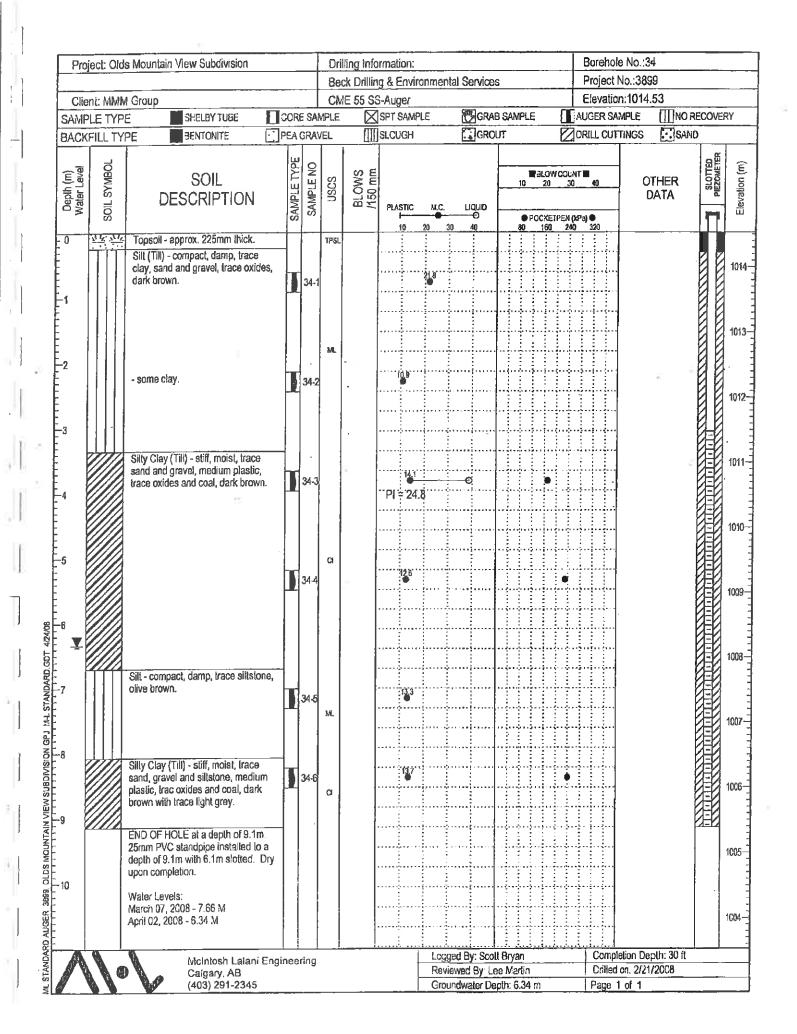
	ject: Old	s Mountain View Subdivision				ling Info								_		ble No.:3			
		1.0			-	ck Drilling		ronmer	Nal Se	rvices	i					No.:38			·
	ent: MMA		COR			IE 55 SS	-Auger SPT SAM		500		0.0.0.0		ſ			on:1019			
	PLE TYP						-			GRAB		12				AMPLE		RECOV	ERY
BACK	FILL TY		PEA	GRAN	/EL		SLOUGH	<u> </u>		GROL	11. 11.		_ (TTINGS	SA		
Depth (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO	USCS	BLOWS /150 mm	PLASTIC	M.C. 20		luid D		0 DPO(LOW CO 20 20 20 20 20 20 20 20 20 20 20 20 20	30	40		OTHER DATA		
0	34-34	Topsoil - approx. 100mm thick.			TPSC				30 4			:	100	24U	320	1		-	10
1		Silt (Till) - compact, dry, trace clay, sand and gravel, trace oxides and coal, medium brown, - some sand.		30-1	M		•									[SO4] = 0.02%		10
2		Sitty Clay (Till) - stiff, damp, trace sand and gravel, medium plastic, trace oxides and coal, medium brown.		30-2		-	1).6									×			10
		- moist.		30-3	27 - -	-							ě						10
		- dark brownish grey.	J	30-4	a														10
		- dark grey.	J	30-5		•				·····							į		10 ⁴
		- trace sandstone.		30-6						· · · · · · · · · · · · · · · · · · ·			•						101
0		END OF HOLE at a depth of 9.1m. 25mm PVC standpipe installed to a depth of 9.1m with 6.1m stolted. Dr upon completion. Water Levels : March 07, 2008 - Dry to 8.74m April 02, 2008 - Dry to 8.75m	y			•••													101 166
		A		1			<u></u>	<u></u>		San .		<u>i</u>			<u></u>	ation D-	10. 20 2		
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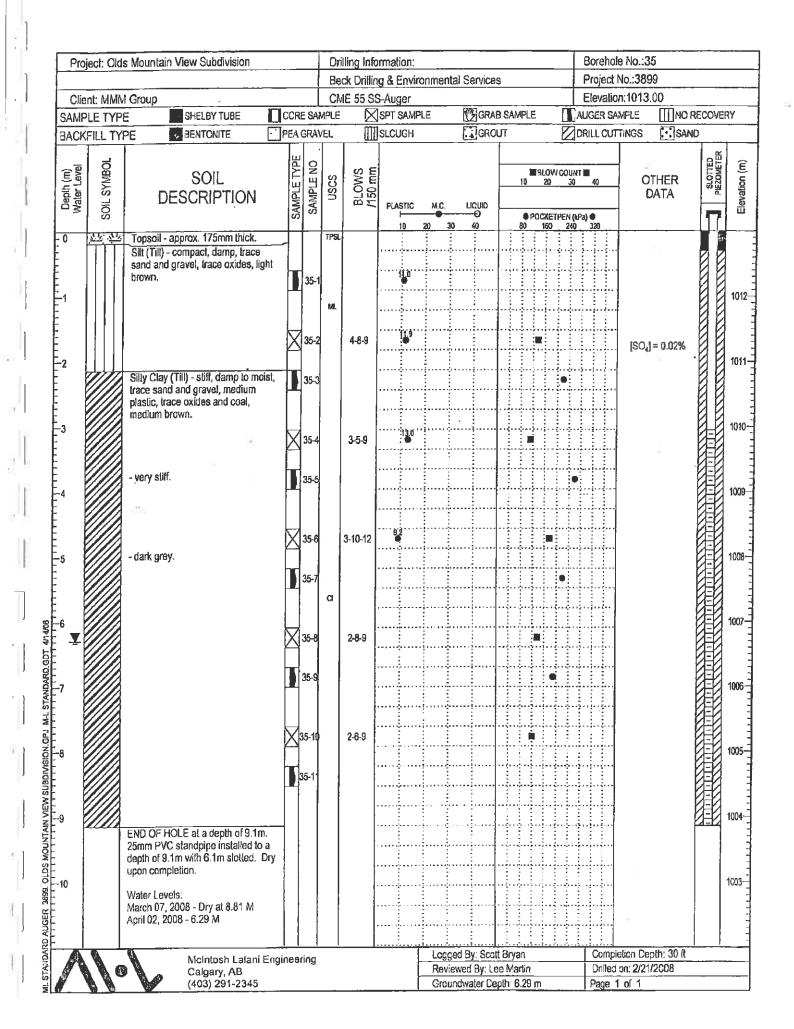
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Pro	ject: Olds	s Mountain View Subdivision					rmation: g & Enviro	oment	ol Service			le No.:36 No.:3899		
Clie	nt: MMM	Group			-	AE 55 SS		ANN GIR			Elevatio			
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	FILL TY		PEA				SLOUGH	-,,	GRC			ITINGS	SAND	
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0	<u>x Ir</u> <u>x Ir</u>	Topsoil - approx, 405mm thick.			TPSL									
1		Silt (Till) - compact, damp to moist trace sand, clay and gravel, trace oxides, medium brown.		44-1	ML.							. Clay % = 1 = 51, Sand	4, Silt % I % = 35	
2		Silly Clay (Till) - stiff, moist, trace sand and gravel, medium plastic, trace oxides and coal, medium brown.		44-2	α	•	119.					à		
4	•	END OF HOLE at a depth of 3.0m. 25mm PVC standpipe installed to a depth of 3.0m with 1.8m slotted. D upon completion. Water Levels: March 07, 2008 - Dry to 2.94m April 02, 2008 - Dry to 2.93m	a)ry			2								
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A		McIntosh Lalani E	Inginee	ering					ed By: Sco ew ed By: L			delion Depth		
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Piujec	Cids Mount	Drilling Information: Beck Drilling & Environmental Services								Borehole No.:37							
Client	/MM Group		.		eck Drillin ME 55 St			rment	a Ser	vices	5		Project No.:3899 Elevation:				
SAMPLE		SHELBY TUBE	CORES			SPT S		F		GRAE	B SAMPLE	Π	AUGER S			ECOVE	2
BACKFIL		* BENTONITE	PEA GR			SLOL			and the second second				DRILL CU				-
Depth (m)		SOIL DESCRIPTION	SAMPLE TYPE	USCS	0.5	PLA	STIC	M.C.		0	10	LOWCOU 20 3 CKETPEN 160 24	N7 🖬 D 40	0	THER DATA		
0 3 	Sill (Ti sand a mediuu - trace Silty C sand a trace o brown.	ay (Till) - stiff, damp, trace nd gravel, medium plastic, xides and coal, medium FHOLE at a depth of 3.0n PVC standpipe installed to of 3.0m with 1.8m slotted. ompletion.	n. 37	a							Bryan			- Clay % = 42, S	= 22, Silt % and % = 36		

Liebe Uniting & Environments Bahnoss Product Association SAMPLE TYPE Betters TURE Once SAMPLE Clores SAMPLE	Project: Olds	s Mountain View Subdivision		Drilling Information: Beck Drilling & Environmental Services									Borehole No.:38							
SAMPLE TYPE SHELEY TUPE CORE SAMPLE SPI SAMPLE CAUGER SAMPLE INORECOVER BACKFILL TYPE SENTONITE PEA GRAVEL SOUL DRILL CUTTINGS SAMPLE DORECOVER GE SOUL DESCRIPTION SUBJECTIVE PEA GRAVEL SOUCH DRILL CUTTINGS SAMPLE 0 SOUL DESCRIPTION SUBJECTIVE SUBJECTIVE PEAGRAVEL SUBJECTIVE OTHER 0 SUBJECTIVE DESCRIPTION SUBJECTIVE PEAGRAVEL SUBJECTIVE OTHER DATA 0 SUBJECTIVE DESCRIPTION SUBJECTIVE PEAGRAVEL SUBJECTIVE OTHER DATA 0 SUBJECTIVE Cauge standard gravel, vace exides, medum brown. SUBJECTIVE SUBJECTIVE OTHER DATA 3 SUBJECTIVE	Client: MMW							onmer	ital Ser	VICES				_	Project No.:3899 Elevation:					
BACKFILL TYPE SENTENTE PEA GRAVEL III SLOUGH GROUT Delluc DUTTINES SAND Image: Solut Stress of the			CORE					<u>ላ</u> ይ	КУ	GRAE	SAMP	νLE		_			E M	NOR	ECOVE	ERY
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0 25-320 Topsoil- approx. 150mm thick Sill (Till) - compact, damp, trace ital 1 Sill (Till) - compact, damp, trace 2 Sill (Till) - compact, damp, trace 1 Sill (Sill (Till) - compact, damp, medium 1 Topsoil, trace oxides and coat, 1 Independent of 3.0m, 2 END OF HOLE at a depih of 3.0m, 2 Sim PVC standpipe installed to a 4 Water Levels: March 07, 2008 - Dry to 3.0m April 02, 2008 - Dry to 2.98m 5 Sim PV of 2.98m	Depih (m) SOIL SYMBOL	DESCRIPTION	SAMPLE TYPE			/150 mm						0 :	20	30	40				PIEZOMETER	
9 10 McIntosh Lalani Engineering Logged By: Socit Bryan Completion Cepth: 10 ft		Stil (Till) - compact, damp, trace clay, sand and gravel, trace oxide medium brown. - some clay. Silly Clay (Till) - stiff, damp to mo trace sand and gravel, medium plastic, trace oxides and coal, medium brown. - trace precipitates. END OF HOLE at a depth of 3.0m 25mm PVC standpipe installed to depth of 3.0m with 1.8m stotted. upon completion. Water Levels: March 07, 2008 - Dry to 3.0m April 02, 2008 - Dry to 2.98m	ist. a Dry	8-2	C		50													

Project: Ok	ds Mountain View Subdivision		Drilling Information: Beck Drilling & Environmental Services								Borehole No.:39 Project No.:3899					
Client: MM	M Group				IE 55 S							Elevation:				
SAMPLE TYP			RE SA			SPT SAM		GRA	R SAM		TE.	AUGER S/		R ON []]	FCOVE	
		PE.				SLOUGH						DRILL CUT	_	SANC	_	
BACKFILL T		<u> </u>	A GRA	VEL T	<u> </u>	aLUUGH		Lafono	1				TINGS	SAUNL		-
Depth (m) SOIL SYMBOL	SOIL DESCRIPTION		SAMPLE IYPE	uscs	BLOWS /150 mm	<i> </i>	M.C.	LIQUID		POCKET	30	40 Pa) ●		THER DATA	PIEZOMETER	
0 22 34	Topsoil - approx. 150mm thick.		+	TPSL		10	20 30	40	8	0 160	240	320	¦			
-1 -2 -3 -4 -5 -6 -7	Silt (Till) - compact, damp, trace sand, clay and gravel, trace oxid medium brown. - some clay. Silty Clay (Till) - stilf, damp to me trace sand and gravel, low plasti trace oxides and coal, medium brown. - medium plastic. END OF HOLE at a depth of 3.0/ 25mm PVC standpipe installed to depth of 3.0m with 1.5m slotted. upon completion. Water Levels: March 07, 2008 - Dry to 2.92m April 02, 2008 - Dry to 2.94m	n.	39-1	CL-ML									Clay % = 40, S	= 13, Silt % and % = 47		
-7 -8 -9 -10	McIntosh Lalani Calgary, AB	Engine	Pring					d By: Scot					letion De	pth: 10 ft /2008		

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					ck Drillin			nmenta	al Serv	ices	3		Project No.:3899				
Client: MM					1E 55 SS				ഞ്ഞം				Elevali		IIII vo a		
SAMPLE TY		CCR						Ľ				AUGER SA				D RECOVER	
BACKFILL T		PEA	GRAN T	/EC	<u>Ції</u> Т	jslouk T	SH	_	<u>.</u> 6	KCL			DRILL CU	TINGS	SAN	- T	
Depth (m) SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO	uscs	BLOWS /150 mm	PLAS	TIC	м.с.	LIQUI	D		30	40		other Data		
0 34.30	Topsoil - approx. 125mm thick.			TPSL		10) 2	0 30	-		● PCCKETPE 80 160	240	KPaj o <u>320</u>	<u> </u>			
	Silt (Till) - compact, dry, some sai trace gravel, trace oxides, light brown. Silty Clay (Till) - stiff, moist, trace sand and gravel, medium plastic, trace oxides and coal, medium brown. END OF HOLE at a depth of 3.0m 25mm PVC standpipe installed to depth of 3.0m with 1.5m slotled. (upon completion. Water Levels: March 07, 2008 - Dry to 2.92m April 02, 2008 - Dry to 2.93m		40-1	ML										Clay % = 51, \$	a = 13, Sill % Sand % = 36		
-8																	
10																	

		s Mountain View Subdivision				g & Enviro	nmenta	Services	S	Project No.:3899				
	nt: MMM		П ас-7 -		<u>/E 55 SS</u>			Racar	B SAMPLE	Elevation:				
	LETYP		CCRE S			SPT SAMPL		GRA		DRILL CUT				
BACK	FILL TY	PE BENTCNITE		WEL	<u>।</u> सि	Jouwen						1		
Depth (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	USCS	BLOWS /150 mm	PLASTIC	M.C.			0 40	OTHER DATA	SLOTTED		
	1. 26	Topsoil - approx. 175mm thick.		TPSL		10	20 <u>30</u>	40	0 20CKETPEN 80 160 24	10 <u>320</u>	· .	┢		
		Sill (Till) - compact, damp, trace sand and gravel, trace oxides, medium brown.	4	1-1		11.4					. Clay % = 17, Sill % = 49, Sand % = 34			
				ML 										
-2		Silly Clay (Till) - stiff, damp to m trace sand and gravel, medium plastic, trace oxides and coal, medium brown.	oist, 1 4	1-2 a.	-						1 1			
-3		END OF HOLE at a depth of 3.0 25mm PVC standpipe installed depth of 3.0m with 1.5m slotted, upon completion.	toa [• •			
4		Water Levels: March 07, 2008 - Dry to 2.92m April 02, 2008 - Dry to 2.92m					,				15			
-5														
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1														
7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1														
10 11 - 1 - 1 - 1 10														
		McIntosh Lalar Calgary, AB	i Engineeri	ng				d By: Sco	tt Bryan ee Martin		d cn. 2/21/2008			

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APPENDIX B

DESIGN AND CONSTRUCTION GUIDELINES

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BACKFILL MATERIALS AND COMPACTION

Maximum density, as used in this section, means Standard Proctor Maximum Dry Density (ASTM Test D698) unless specified noted otherwise. Optimum moisture content is as defined in this text.

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"General engineered fill" materials should comprise clean, well-graded granular soils or inorganic, low-plastic cohesive soils. Such material should be placed in compacted lifts not exceeding 200 mm and compacted to not less than 98 percent of maximum density, at a moisture content at or slightly above optimum.

"Structural fill" materials should comprise clean, well-graded inorganic granular soils. Such fill should be placed in compacted lifts not exceeding 150 mm and compacted to not less than 98 percent of maximum density, at a moisture content at or slightly (0 to 3 percent) above optimum.

"Landscape fill" material may comprise soils without regard to engineering quality. Such soils should be placed in compacted lifts not exceeding 300 mm and compacted to a density of not less than 90 percent of maximum density.

Backfill adjacent to and above footings, abutment walls, basement walls, grade beams and pile caps or below highway, street or parking lot pavement sections should comprise general engineered fill materials as defined above.

Backfill supporting structural loads should comprise structural fill materials as defined above.

Backfill adjacent to exterior footings, foundation walls, grade beams and pile caps and within 300 mm of final grade should comprise low-plastic cohesive general engineered fill as defined above. Such backfill should provide a relatively impervious surface layer to reduce seepage in the sub-soil.

Backfill should not be placed against a foundation structure until the structure has sufficient strength to withstand the earth pressures resulting from placement and compaction. During compaction, careful observation of the foundation wall for deflection should be carried out continuously. Where deflection is apparent, the compactive effort should be reduced accordingly. In order to reduce potential compaction induced stresses, only hand held compaction equipment should be used in the compaction of fill within 500 mm of retaining walls or basement walls.

Backfill materials should not be placed in a frozen state or placed on a frozen subgrade. All lumps of materials should be broken down during placement.

Where the maximum-sized particles in any backfill material exceed 50 percent of the lift thickness or minimum dimension of the cross-section to be backfilled, such particles should be removed and placed at other more suitable locations on site or screened-off to delivery to site.

Bonding should be provided between backfill lifts, if the previous life has become desiccated. For fine-grained materials, the previous lift should be scarified to 75 mm in depth followed by proper moisture conditioning and recompaction.

Recommendations for the specifications for various backfill types are presented below.

SIEVE SIZES (SQUARE OPENINGS)	PERCENT PASSING BY WEIGHT					
. 200 mm	100 of Total Sample					
150 mm	96 - 100 of Total Sample					
75 mm	60 - 80 of Total Sample					
25 mm	70 - 100 of Material Passing 75 mm Sieve					
4.75 mm	25 - 63 of Material Passing 75 mm Sieve					
1.18 mm	14 - 41 of Material Passing 75 mm Sieve					
0.60 mm	7 - 30 of Material Passing 75 mm Sieve					
0.15 mm	3 - 18 of Material Passing 75 mm Sieve					
0.075 mm	2 - 9 of Material Passing 75 mm Sieve					

"Clean, well-graded inorganic granular soils" should conform to the following grading:

Any grading variation from the above should be at the discretion of the Engineer; however, the percent of material passing the 0.075 mm sieve size should not exceed % of the material passing the 0.6 mm sieve. The pit-run gravel should be free of any form of coating and any gravel containing clay, loam or other deleterious materials should be rejected. No oversized material should be tolerated.

"Crushed gravel", should conform to the following grading:

	1101/111	AL UKAYEL BILL	
SIEVE SIZES (SQUARE OPENINGS)	100 mm	50 mm	25 mm
100 mm	100		
75 mm	90 - 100		
50 mm		100	
40 mm	60 - 80	90 - 100	
- 25 mm			100
20 mm	40 - 66	50 - 75	95 - 100
10 mm	25 - 54	25 - 52	60 - 80
4.75 mm	15 - 43	15 - 40	40 - 60
2.36 mm	10 - 35	10 - 33	28 - 48
0.60 mm	5 - 23	5 - 23	13 - 29
0.30 mm		 :	9 - 21
0.15 mm	3 - 12	2 - 14	6 - 15
0.075 mm	2 - 10	1 - 10	4 - 10

PERCENT PASSING BY WEIGHT NOMINAL GRAVEL SIZE

Gravel:

100 mm Crushed Gravel: At least 13 percent by weight of the material retained on the 4.75 mm sieve should have two more fractured faces.

50 mm Crushed Gravel: At least 13 percent by weight of the material retained on the 4.75 mm sieve should have two more fractured faces.

25 mm Crushed Gravel: At least 50 percent by weight of the material retained on the 4.75 mm sieve should have two more fractured faces.

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Any gravel containing deleterious material should be rejected.

"Coarse gravel" for bedding and drainage should conform to the following grading:

SIEVE SIZES (SQUARE - OPENINGS)	50 mm	40 mm
50 mm	100	
40 mm	90 - 100	100
25 mm		95 - 100
20 mm	35 - 70	
15 mm		25 - 60
10 mm	10 - 30	
4.75 mm	0 - 5	0 - 10
2.36 mm		0 - 5

PERCENT PASSING BY WEIGHT (NOMINAL GRAVEL SIZE)

"Coarse sand" for bedding and drainage should conform to the following grading:

SIEVE SIZES (SQUARE OPENINGS)	PERCENT PASSING BY WEIGHT
10 mm	100
4.75 mm	95 - 100
2.36 mm	80 - 100
1.18 mm	50 - 85
0.60 mm	25 - 60
0.30 mm	10 - 30
0.15 mm	2 - 10

"Lean-mix concrete" should be low strength concrete having a minimum 28 days compressive strength of 3.5 MPa.

CONSTRUCTION EXCAVATIONS

Construction should be in accordance with good practice and comply with the requirements of the responsible agencies.

All excavations greater than 1.5 m deep should be sloped or shored for work protection.

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Shallow excavations up to 3 m depth may use temporary side slopes of 1H:1V. A flatter slope of 2H:1V should be used if groundwater is encountered. Localized sloughing can be expected from these slopes.

Deep excavations or trenches may require temporary support if space limitations or economic considerations preclude the use of sloped excavations.

For excavations greater than 3 m depth, temporary support should be designed by a qualified geotechnical engineer. The design and proposed installation and construction procedures should be submitted to McIntosh•Lalani Engineering Ltd. for review.

The construction of a temporary support system should be monitored. Detailed records should be taken of installation methods, materials, in situ conditions and the movement of the system. If anchors are used, they should be load tested. McIntosh•Lalani Engineering Ltd. can provide further information on monitoring and testing procedures, if required.

Attention should be paid to structures or buried service lines close to the excavation. For structures, a general guideline is that if a line projected down at 45° from a horizontal, from the base of foundations of adjacent structures, intersects the extent of the proposed excavation, then these structures may require underpinning or special shoring techniques to avoid damaging earth movements. The need for any underpinning or special shoring techniques and the scope of monitoring required can be determined when details of the service ducts and vaults, foundation configuration of existing buildings and final design excavation levels are known.

No surface surcharges should be placed closer to the edge of the excavation than a distance equal to the depth of the excavation, unless the excavation support system has been designed to accommodate such surcharge.

SHALLOW FOUNDATIONS

Design and construction of shallow foundations should comply with relevant Building Code requirements.

The term "shallow foundations" includes strip and spread footings, mat slab and raft foundations.

Minimum footing dimensions in plan should be 0.45 m and 0.9 m for strip and square footings, respectively.

No loose, disturbed or sloughed material should be allowed to remain in open foundation excavations. Hand cleaning should be undertaken to prepare an acceptable bearing surface. Recompaction of disturbed or loosened bearing surface may be required.

Foundation excavation and bearing surfaces should be protected from rain, snow, freezing temperatures, drying and the ingress of free water, during and after footing construction,

Footing excavations should be carried down into the designated bearing stratum.

After the bearing surface is approved, a mud slab should be poured to protect the soil and provide a working surface for construction, should immediate foundation construction not be intended.

All constructed foundations should be placed on unfrozen soils, which should be at all times protected from frost penetration.

All foundation excavations and bearing surface should be observed by a qualified geotechnical engineer to confirm that the recommendations contained in this report have been followed and that soil conditions are consistent with those assumed in the design.

Where over-excavation has been carried out through a weak or unsuitable stratum to reach into a suitable bearing stratum or where a foundation pad is to be placed above stripped natural ground surface, such over-excavation may be backfilled to subgrade elevation utilizing either structural fill or lean-mix concrete. These materials are defined under the separate heading "Backfill Materials and Compaction."

APPENDIX F2

2024 Watt -

Geotechnical Report



Environmental and Remediation Services Inc.



NETOOK CROSSING

Geotechnical Assessment

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Author

Jason Deschamps, P.Eng.

Reviewer

Prepared For:B & A Planning GroupDate:2024-03-19Our File No.:3903.T01

WATT CONSULTING GROUP 1300 – 736 6th Ave SW Calgary, AB T2P 3T7 (403) 273-9001



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APPENDICES

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1.0 INTRODUCTION

Watt Consulting Group (WATT) was retained by B&A Planning Group to complete a geotechnical assessment to support development within the Netook Crossing subdivision. The objective of the geotechnical assessment was to determine the subsurface ground and groundwater conditions at the project site, and to provide geotechnical comments and recommendations pertinent to project design and construction.

2.0 PROJECT BACKGROUND

The project site is located east of Olds, Alberta, North of Highway 27, West of Range Road 12, and South of the Olds Golf Club. The site is a currently undeveloped quarter section, used for agriculture activities.

Based on a review of published geological data and our local experience, the subsurface ground conditions at the project site are anticipated to comprise of clay till, underlain by completely to highly weathered bedrock.

A geotechnical investigation is required to support development and building permit applications, and to provide comments and recommendations for foundation design and other development features.

3.0 GEOTECHNICAL INVESTIGATION

3.1 Investigation Methodology

During a previous Geotechnical Investigation by MacIntosh Lalani in 2008, nine boreholes were drilled within the project area. To comply with the County spacing requirements, an additional twenty seven boreholes were completed, representing a total of thirty six boreholes on the subject property. On December 1 and 2, 2023, WATT staff oversaw the drilling of twenty seven geotechnical boreholes at the approximate locations shown on Figure 1 – Borehole Location Plan, attached in Appendix A. Borehole locations were selected based on site access and locations of underground and overhead utilities at time of drilling. Drilling was carried out by Venom Drilling of Blackfalds, Alberta, using a truck mounted solid stem auger drill rig. All boreholes were advanced to the design depth of 6 meters below ground surface (mbgs), with the exception of BH23-04 which reached early refusal. Standard penetration Tests (SPTs) were completed at select intervals, and soil samples were taken from the split spoon sampler and from the auger flight.

The subsurface ground and groundwater conditions were logged in the field by WATT staff as drilling proceeded. The subsurface stratigraphy encountered is shown on the



Borehole Records attached in Appendix B. 25 mm diameter standpipe piezometers were installed in each of the boreholes.

Soil samples obtained during drilling were submitted to Solum Consultants Ltd. Geotechnical and Materials Testing Laboratory in Calgary, Alberta. The following soil index tests were completed on select soil samples:

- Moisture content determination (ASTM D2216) 159 tests;
- Particle size analysis (ASTM D422) 5 tests;
- Atterberg limits (ASTM D4318) 6 tests;
- Water soluble sulphate concentrations (CSA A23.1) 4 tests; and
- California Bearing Ratio (CBR) 1 test.

The soils laboratory test results are shown on the Borehole Records, are attached in Appendix C, and are discussed in Section 3.2.

3.2 Subsurface Ground Conditions

The subsurface stratigraphy encountered at the discrete borehole locations generally comprised of topsoil and fill, underlain by silty clay till and completely to highly weathered bedrock. The Borehole Records attached to this report present WATT's interpretation of the materials encountered. It is noted that the subsurface stratigraphy may be variable between borehole locations. A description of the subsurface soil strata encountered is provided in the following sections.

3.2.1 Topsoil

Topsoil was encountered in all 27 holes, ranging in depth from 0.2 to 0.3 metres.

3.2.2 Silty Clay Till

Silty clay till was the predominant material encountered in all boreholes. The till was light brown to grey in color, contained some sand and trace gravel. Field records indicate the silty clay is low to medium plasticity and was damp to moist. Oxidized stains were observed at variable depths, indicating groundwater influence or infiltration of surface water.

SPTs completed within the silty clay till stratum resulted in N-values ranging from 7 to 32 blows per 300 mm of penetration, indicating the material is firm to hard. Moisture content tests completed within the silty clay till ranged from 9% to 19%, indicating damp to wet sample conditions. A summary of particle size distribution and Atterberg Limits Test (plasticity) are shown below:



		Atterberg	g Limits		Particle S	Size		
Borehole ID	Depth (m)	Liquid Limit	Plastic Limit	Plasticity Index	Gravel (%)	Sand (%)	Silt (%)	Clay (%)
BH23-03	2.0	26	17	9	-	-	-	-
BH23-04	2.0	32	17	15	-	-	-	-
BH23-06	2.0	38	15	23				
BH23-08	3.0	-	-	-	0	34	48	18
BH23-11	2.0	37	15	22				
BH23-11	3.0	-	-	-	2	31	47	21
BH23-15	2.0	34	14	20	-	-	-	-
BH23-16	1.0	-	-	-	2	36	41	21
BH23-18	2.0	-	-	-	0	32	42	26
BH23-19	2.0	34	14	20	-	-	-	-
BH23-24	3.0	-	-	-	1	34	42	24

Table 1: Soil	s Index Test	: Results – Silt	v Clav Till
1 4 5 1 6 6 1 1		enter enter	

3.2.3 Silty Sand (Completely Weathered Bedrock)

Silty sand was observed in 12 of the 27 boreholes, typically underlying the topsoil. The silty sand was noted to contain traces of clay and gravel and described as light brown, still and low plasticity.

Three SPTs completed within the silty sand stratum resulted in N-values ranging from 10 to 13 blows per 150 mm, indicating the material is stiff. Moisture content tests completed on SPT and auger samples ranged from 9% to 13%, indicating dry to damp sample conditions.



3.3 Subsurface Groundwater Conditions

During the subsurface investigation on December 1 and 2, 2023, standpipe piezometers were installed in each borehole to monitor groundwater levels. The piezometers were subsequently damaged and unable to be read. To allow determination of the stabilized groundwater elevation, the 27 piezometers were re-installed on February 8, 2024.

Very little groundwater seepage was observed in all boreholes and each borehole was noted to be dry upon the completion of drilling. It should be recognized that groundwater levels vary seasonally and from year to year, and are dependent on many factors including surface drainage, precipitation and the hydrology of the area. Groundwater conditions may also change over time due to site development, such as new building construction or site re-grading.

The installed standpipes will continue to be read to determine the stabilized groundwater elevation and a follow-up report with this information will be provided. For preliminary purposes, the coefficient of permeability of the silty clay till may be taken as $k\sim 1*10^{-7}$ m/s.

Since standpipe piezometers were re-installed on February 8, 2024, they have continued to be read frequently to determine the groundwater elevation at each location. The below table summarizes the groundwater readings to date, indicating the highest groundwater recorded and corresponding elevation for each borehole:

Borehole ID	Surface Elevation (masl)	Highest Depth to Water Recorded (m)	Maximum Groundwater Elevation (masl)	
BH23-01	1018.8	2.5	1016.3	
BH23-02	1019.0	2.7	1016.3	
BH23-03	1019.3	1014.9		
BH23-04	1018.3	2.0	1016.3	
BH23-05	1020.3	Dry	N/A	
BH23-06	1018.6	3.1	1015.5	
BH23-07	1018.5	3.5	1015.0	
BH23-08	1018.1	2.2	1015.9	

Table 2: Water Level Readings – Summary to Date



Borehole ID	Surface Elevation (masl)	Highest Depth to Water Recorded (m)	Maximum Groundwater Elevation (masl)
BH23-09	1019.4	Dry	N/A
BH23-10	1019.6	4.1	1015.5
BH23-11	1019.5	4.4	1015.1
BH23-12	1018.9	Dry	N/A
BH23-13	1018.7	4.6	1014.1
BH23-14	1020.4	Dry	N/A
BH23-15	1019.5	Dry	N/A
BH23-16	1019.6	5.6	1014.0
BH23-17	1018.8	Dry	N/A
BH23-18	1019.5	Dry	N/A
BH23-19	1018.3	3.9	1014.4
BH23-20	1019.9	5.0	1014.9
BH23-21	1019.4	5.0	1014.4
BH23-22	1018.2	Dry	N/A
BH23-23	1018.9	Dry	N/A
BH23-24	1019.3	Dry	N/A
BH23-25	1018.5	4.7	1013.8
BH23-26	1018.0	Dry	N/A
BH23-27	1019.0	Dry	N/A



4.0 GEOTECHNICAL COMMENTS AND RECOMMENDATIONS

4.1 General Geotechnical Commentary

Design and construction recommendations pertaining to the geotechnical aspects of the proposed development are provided in this report section based on the results of the geotechnical evaluation fieldwork, the laboratory testing carried out, and WATT's understanding of the proposed development at time of report preparation. These recommendations are intended to provide support for various project concepts and specifications as well as insight to determine the most appropriate site-specific construction methodologies. As well, WATT should be retained to review applicable geotechnical aspects of the final design (drawings and specifications) and provide all necessary field reviews.

The subsurface ground and groundwater conditions encountered at the project site are considered suitable for the proposed development. Geotechnical considerations for the project site are summarized as follows:

- Competent foundation materials in form of silty clay till were encountered at the project site. The materials are suitable to support shallow foundations in form of spread and strip footings.
- Discussions and recommendations regarding groundwater will be provided in the follow-up report once stabilized groundwater elevations are available.

Detailed design and construction comments and recommendations for the proposed development are provided in the following Sections.

4.2 Site Preparation

All deleterious material such as, but not limited to, surface vegetation and organic soils as well as all fill soils should be sub-excavated to competent, minimum stiff silty clay till subgrade material.

Prior to any development activities, all exposed subgrade surfaces subject to site development should be proof-rolled using heavy equipment such as a loaded tandem dump truck. All loose or soft areas must be sub-excavated to competent material and replaced with approved engineered fill. Further recommendations for backfill materials (types, re-use of site soils) and compaction requirements are provided in Section 4.3. The final subgrade surface should be carefully graded to prevent ponding and to direct water away from the building area.



It is recommended to carry out construction during the spring, summer and fall months. If construction is carried out during winter conditions, the subgrade should be protected from freezing. In addition, the subgrade should be protected from wetting or drying, both before and after the placement of engineered fill, granular base material, or concrete. Subgrade surfaces that are allowed to dry or become wet should be scarified, moisture conditioned, and re-compacted.

4.3 Backfill and Compaction

The native silty clay till soils encountered at the project site are generally suitable for reuse as engineered fill. All engineered fill should be placed in lifts not exceeding 200 mm thickness (loose measure) and should be compacted to minimum 98% of Standard Proctor maximum dry density (SPMDD), at a moisture content of 0 to +2% of its optimum moisture content (OMC) for compaction purposes. The maximum lift thickness may vary depending on the compaction equipment used and should be verified through field density testing at time of construction. It is noted that underlying completely weathered silty sand bedrock is likely not suitable for re-use as engineered fill, due to the high silt content and associated difficulty to achieve optimum moisture content for compaction purposes.

Structural fill should comprise of well graded, 25 mm minus crushed gravel. It should be placed in lifts not exceeding 200 mm thickness (loose measure) and should be compacted to minimum 100% of SPMDD, at a moisture content of \pm 3% of OMC.

All fill must be free from topsoil, organics, fill and otherwise deleterious material, and must not be frozen at time of placement.

4.4 Strip and Spread Footings

This Section provides geotechnical design parameters in Limit States Design format as per National Building Code of Canada – 2019 Alberta Edition. As outlined above, conventional spread and strip footings are considered suitable for the proposed building. It is anticipated that footings will be within the silty clay till material.

The following geotechnical foundation design recommendations are based on the foundation dimensions ranging from 0.5 to 2.0 m widths, and a minimum embedment depth of 0.5 m below ground level (measured from ground surface or top of slab-on-grade, whichever is less). Increased embedment depths will be needed to provide adequate soil cover for frost protection purposes (see Section 4.8).

Values for the factored Ultimate Limit States (ULS) and Serviceability Limit States (SLS) geotechnical bearing resistances for bearing capacities for shallow foundations with



above noted dimensions may be taken as 250 kPa and 150 kPa respectively. A resistance factor of 0.5 as per Canadian Building Code has been applied to determine the factored bearing resistance at ULS conditions. SLS bearing capacities were determined based on typical tolerable total and differential settlement of 25 mm and 20 mm, respectively.

For larger footings, the geotechnical bearing resistance would generally increase. However, settlement of the footings would also increase and add to the high risk of excessive total and differential settlement for the building structure. WATT would be pleased to complete additional analysis and provide further geotechnical input should footings with more than 2.0 m width be required.

The values presented above are for vertical, concentric loading, as described in the CFEM (2006). For footings subjected to eccentric loads, the following equivalent footing width should be used to calculate the bearing pressure of the footing:

Where B' is the equivalent footing width; B is the actual footing width; L' is the equivalent footing length, L is the actual footing length, and e is the eccentricity of the load. Effects of inclined loads, if any, should also be considered as discussed in the CFEM (2006).

The subgrade surfaces beneath building foundations must be free from frozen, loose or soft materials. The base of all footings must be inspected by qualified geotechnical personnel prior to placing concrete to confirm the above design bearing pressures and to ensure there are no disturbances or deleterious materials present.

4.5 Non-Structural Floor Slabs-on-Grade

Non-structural cast-in-place concrete slabs-on-grade, placed on approved subgrade soils, are typically used as floor systems. A 150 mm thick levelling course comprising of 25 mm minus crushed gravel (similar to structural fill, see Section 4.3) should be placed below non-structural slab-on-grades. The crushed gravel levelling course should be placed within $\pm 3\%$ of its optimum moisture content for compaction purposes (OMC) and compacted to minimum 100% of its Standard Proctor maximum dry density (SPMDD). It is recommended to place a non-woven geotextile separation membrane between cohesive engineered fill and granular fill.

Vertical differential movements between non-structural floor slabs-on-grade and structural building elements are inevitable and considered to be acceptable as per the current standard of practice. Slabs should float on the subgrade and only be tied into the foundation walls or grade beams at doorways. To reduce the effects of vertical slab



movement (e.g. potential slab cracking, partition wall distortion, cracking of brittle finishing surfaces), the following provisions should be implemented to allow the slab to move independently of the structural components of the building:

- Partition and non-bearing walls should not be rigidly connected to bearing walls or columns;
- Reinforce the concrete and articulate the slab at regular intervals to control cracking;
- Heating ducts placed beneath the floor slab should be insulated to minimize drying and shrinkage of clay fill/till soils; and
- Piping and electrical conduits should permit flexibility and some movement.

Non-structural slabs-on-grade supported by fill (i.e. backfill placed surrounding basement walls) are not recommended as consolidation settlement of fill may occur. These areas should be design as suspended slabs, supported by basement walls and surrounding footings.

It is noted that the basement floor slab may also be designed as a structural (raft) slabon-grade, which would reduce effort for detail footing excavations underneath a nonstructural slab-on grade. WATT would be pleased to provide parameters for raft foundation design should this option be considered for this project.

4.6 Lateral Earth Pressures

Lateral pressures are to be considered acting on below-grade building perimeter walls. The earth pressures will be induced by new fill placed within basement excavation, which is anticipated to comprise of local silty clay till, or imported soil of similar nature.

Active earth pressure conditions should be used in establishing earth pressures acting on the underground structure walls. The lateral pressure applied to subgrade walls is calculated using the following formula:

$$P = K \left(\gamma b H + q \right)$$

Where:

P = lateral earth pressure (kPa)

K = earth pressure coefficient

 $\gamma_{\rm b}$ = soil unit weight

H = Height of wall (m)

q = surcharge load (if applicable)



An earth pressure coefficient of $K_a = 0.40$ may be used for active earth pressure conditions. The soil unit weights for the re-worked silty clay till may be taken as 19 kN/m³ above the groundwater table.

The equation for lateral earth pressure assumes a horizontal ground surface behind the buried wall. If the ground surface slopes away from the wall, design pressure should be re-evaluated. Hydrostatic pressures acting on below grade walls may also be considered in design, depending on the selected waterproofing/dewatering method (see Section **Error! Reference source not found.**).

4.7 Seismic Considerations

Seismic design for residential structures is based on the National Building Code of Canada (NBCC). The primary objective of the NBCC earthquake resistant design requirements is to protect the life and safety of the building occupants as the building responds to strong ground shaking. Structures designed in conformance with the NBCC provisions may undergo extensive structural damage during strong ground shaking but should not collapse. Collapse is defined to be a state where occupants can no longer exit the building because of structural failure. This implies that supporting foundations necessary to ensure the building's post-earthquake stability must be protected against excessive movement under strong ground shaking.

Based on the results of the field investigation, it is appropriate to classify the ground conditions at the project site as a Class C Site for seismic site response. Liquefaction of the silty clay till soils or completely to highly weathered bedrock encountered at the project site is unlikely.

4.8 Frost Protection

Minimum soil cover of 1.5 and 2.0 m should be provided for heated and unheated structures, respectively. Alternatively, rigid insulation may be used to provide equivalent frost protection. Grade beams that do not have adequate soil cover for frost protection should be constructed with a minimum 100 mm void space below the grade beam. It is noted that the frost penetration depths provided above are based on the native, cohesive soils at the project site. Greater frost depths are to be considered if native materials are being replaced, e.g. if granular fill is used to backfill temporary excavations or utility trenches.

Concrete flatwork should be designed with anticipation of some frost heave occurring. Concrete sidewalks should be dowelled into footings or grade beams in threshold areas where heave of concrete panels would obstruct the proper opening of doors and present tripping hazards. As the outside of edge of these panels will still heave, the panel should



either be properly jointed to control crack locations or reinforced by placement of adequate reinforcing steel. Alternatively, rigid insulation may be placed below flatwork to prevent frost formation in the underlying subgrade. WATT can provide detailed recommendations for such insulation if required.

4.9 Temporary Excavation and Dewatering

Temporary excavations (estimated duration of less than 6 months) will be required to construct the basement and for utility trenches. The excavations for this project site are anticipated to be primarily within native silty clay till soil.

All excavations should follow Alberta Occupational Health and Safety Code Standards, Chapter 32 "Excavation and Tunneling". The subsurface soils encountered at the project site are to be classified as "likely to crack or crumble soil". Excavations of up to 1.5 m depth may be cut vertically into the soil strata. Excavations with greater depth may be sloped to within 1.5 m of the bottom of the excavation at an angle of not less than 45° measured from the vertical. It is anticipated that excavation depths will not exceed approximately 4.0 mbgs. Excavations of greater depth should be subject to a slope stability assessment.

Seepage into the excavation at the project site may occur, depending on the groundwater conditions encountered during construction. Although the boreholes were noted to be dry during drilling, the stabilized groundwater elevation may help to determine the risk of seepage during excavations.

Due to the fine-grained nature of the water bearing ground stratum, temporary excavation side slopes may not be stable without prior lowering of the groundwater level. A suitable dewatering method for the subsurface ground conditions at the project site comprises of a series of vacuum-assisted wellpoints. The wellpoint system should be designed by a qualified dewatering designer/contractor, who may also provide dewatering alternatives based on local experience.

Prior to allowing workers to enter the construction excavations, a thorough inspection should be undertaken for evidence of instability (cracks, bulging, sloughing, seepage, or else). Any loose/unstable soils or cobbles should be scaled from the excavations prior to worker entry. All unsupported excavations should be monitored on a daily basis for evidence of slope movements such as slumping, bulging, or else. Any such movements should be reported to WATT and remedial stability measures undertaken immediately.

Stockpiles of construction materials, excavated soil, construction equipment, or traffic should be kept away from the slope crest/edge by a distance equal to the depth of excavation. The vibration created from heavy machinery operations or compaction



processes can destabilize a slope; hence, use of heavy machinery within close proximity to excavated slopes should be minimized.

Temporary shoring will be required if the aforementioned excavation geometry cannot be facilitated, or deeper excavations are required for construction aspects. A qualified shoring consultant/contractor should be retained to design a suitable shoring system for the project site, if required.

4.10 Site Grading and Drainage

To provide proper drainage for the proposed development and to direct surface water to areas away from proposed structures, final site landscaping grades should be sloped away from building perimeter walls to mitigate the potential of surficial water ponding in localized areas adjacent to structures. Minimum final site grades draining away from building structures of 1.0% in paved areas, 1.5% in non-paved areas, and 3.0% within 2.0 m laterally of structures adjacent to landscaped areas are recommended.

All downspouts should be directed away from the building structure to a site gradient that promotes positive surficial drainage away from the attached building. Downspouts should not be directed into the perimeter drain or weeping tile system (if constructed).

4.11 Pavement Design Considerations

Recommendations for asphaltic concrete structures placed on suitably prepared subgrade soils as outlined in Section 4.2 are provided in the following table:

Material	Minimum Design Thickness (mm)									
Material	Paved Lane	Resident	tial Local	Residential Collector						
Asphalt Concrete	75	75*	90	100						
25 mm Crushed Gravel Base	100	150	150	175						
80 mm Crushed Granular Subbase	300	300	200	300						

Table 3: Recommended Asphaltic Concrete Pavement Structure

*Red Deer County Specifications require a minimum depth of asphaltic concrete on local roads and primary access lanes with deep utility services of 90mm.

Minimum thicknesses have been designed based on a soaked CBR of 3.1%.

Netook Crossing



All materials used to construct asphaltic concrete pavement structures should comply with the Mountain View County Standard Specifications (current edition). Test results verifying materials properties should be provided to WATT to confirm compliance with the specifications prior to use and placement on site.

4.12 Concrete Exposure Class

Four sulphate (SO₄) in groundwater samples, mg/L resulted in sulphate concentrations ranging from 521 to 918 mg/L. The test result indicated negligible exposure to concrete in contact with the subsurface soils. Accordingly, concrete placed in contact with the soil can comprise of Type GU cement. In addition, all concrete must be designed in accordance with CSA A23.1-04 i.e. air-entraining agents are required in freeze/thaw zones. Any imported fill to be placed in contact with concrete should also be tested for water-soluble sulphate content and the above recommendations re-evaluated.

4.13 Review, Testing and Field Inspection

WATT should be given the opportunity to review details of the design and specifications related to geotechnical aspects of this project prior to construction. The recommendations provided in this report should be supported by an adequate scope of field review during construction. All construction should be undertaken by an experienced contractor for the foundation and earthworks construction. As a minimum, an adequate scope of field review is as follows:

- Shallow Foundations → Observation of all bearing surfaces prior to fill or concrete placement;
- Floor Slab-on-Grades → Observation of all subgrades prior to fill or concrete placement;
- Engineered Fill Placement → Full-time monitoring and compaction testing during fill placement;

All geotechnical field reviews must be carried out by a qualified geotechnical engineer or technician independent of the contractor. Failure to provide an adequate level of field review for construction of the foundations may be in contradiction of the Alberta Building Code requirements.



5.0 LIMITATIONS

The recommendations provided in this geotechnical evaluation report are based on the interpreted findings encountered within three (3) geotechnical boreholes drilled across the project site. The subsurface soil and groundwater conditions observed during borehole drilling are anticipated to be reasonably representative of the project site; however, it should be noted that innate variable conditions may be encountered at the time of various construction aspects. WATT should be notified and given the opportunity to re-evaluate current information, if required, should geotechnical conditions other than those reported herein be identified at any stage of development.

This report has been prepared with accepted geotechnical soil and foundation engineering practices/principles for the project details specified within this report. The recommendations presented herein are subject to an adequate level of inspection during construction and any relevant Alberta Building Code requirements, or their validity may be jeopardized. No other warranty is expressed or implied.

6.0 CLOSURE

We trust that the information contained in this report meets your present requirements. Please do not hesitate to contact the undersigned with any questions, or should you require further geotechnical input on this project.

Sincerely,

WATT Consulting Group

Joel Rombough, P.Eng.

Geotechnical Lead

T 403-462-0718



APPENDIX A: FIGURE 1 – BOREHOLE LOCATION PLAN

BH23-01	BH23-02	BH23-03	BH23-04	BH23-05	BH23-06.	A DUTY OF
	BH23-07		BH23-08		BH23-09	
BH23-10	BH23-11	BH23-12	BH23-13	BH23-14	BH23-15	
	BH23-16		BH23-17		BH23-18	
BH23-19	BH23-20	BH23-21	BH23-22	BH23-23	BH23-24	A STATE OF A STATE OF A
27	BH23-25	27	BH23-26		BH23-27	



APPENDIX B: BOREHOLE RECORDS

	Consu	VAT T Iting Group						LL NU	JMBER BH23-01 PAGE 1 OF 1
	T B&A I								
PROJECT NUMBER 3903.T01									
DATE	STARTE	D 2/12/23		PLETE	D _2/2	12/23	GROUND ELEVATION 1018.8 m	HOLE S	IZE 6" Auger
DRILL	ING CON	TRACTOR _	Venom Environme	ntal Dr	illing		GROUND WATER LEVELS:		
DRILL	ING MET	HOD Truck	Mounted Auger				AT TIME OF DRILLING		
LOGG	ED BY	GS	CHEC	KED E	BY _JF	२	AT END OF DRILLING		
NOTES	S						AFTER DRILLING 2.50 m / Elev	1016.30 n	1
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		0.25 (ML) \$	Topsoil Silty sand, trace clay and gravel. Brown, compact, low plasticity.	1018.55	
 	SPT 1	3-5-7 (12)	MC = 16%			1.50 (CL-M to med	IL) Silty clay till, trace sand and gravel. Low dium plastic, brown, damp, stiff to very stiff.	1017.30	
2			MC = 16%	CL- ML		¥		1015 00	
3	SPT 2	3-6-9 (15)	MC = 16%	_		3.00 (CL-M to med	IL) Silty clay till, trace sand and gravel. Low dium plastic, light grey, damp, very stiff.	1015.80	
			MC = 16%						
 5	SPT 3	3-6-11 (17)	MC = 16%	CL- ML					
 6		2.0.40		_					
	SPT 4	3-9-10 (19)	MC = 16%						
						6.45	Rottom of hole at 6.45 m	1012.35	
							Bottom of hole at 6.45 m.		

							WE	LL NU	JMBER BH23-02	
									PAGE 1 OF 1	
	Consul	ting Group)							
	CLIENT B&A Planning									
			.T01							
							GROUND ELEVATION 1019 m	HOLE S	IZE _ 6" Auger	
							GROUND WATER LEVELS:			
			Mounted Auger			2				
										
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1"	
				ОН		0.20 (OH)	Topsoil	1018.80		
	SPT 1	3-3-4 (7)	MC = 15% MC = 16%			(CL-N	L) Silty clay till, trace sand. Low to medium , brown to grey, damp, stiff to very stiff.			
	SPT 2	3-4-6 (10)	MC = 16%	CL- ML						
			MC = 14%							
	SPT 3	3-6-7 (13)								
5	3	(13)	MC = 13%							
	SPT 4	3-5-9 (14)	MC = 15%	-						
		()				6.45	Bottom of hole at 6.45 m.	1012.55		

								WELL NU	JMBER BH23-03	
		VATT							PAGE 1 OF 1	
	Consu	Iting Grou	р							
		Planning					PROJECT NAME _ Netook Crossing			
	PROJECT NUMBER 3903.T01									
							GROUND ELEVATION 1019.3 m	HOLE S	IZE 6" Auger	
							GROUND WATER LEVELS:			
			Mounted Auger			5				
			CHEC							
									•	
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC	
				ОН		0.20 (OH)	Topsoil	1019.10		
	SPT 1	3-3-4 (7)	MC = 15% MC = 14%			(CL-N	IL) Silty clay till, trace sand and gravel dium plastic, brown to grey, damp, stif tiff.	. Low		
	SPT 2	3-5-7 (12)	MC = 15%	CL- ML						
4			MC = 17%			Ā				
	SPT 3	4-6-9 (15)								
			MC = 16%	-						
	SPT 4	4-6-12 (18)	MC = 16%			6.45		1012.85		
					****	12110	Bottom of hole at 6.45 m.	1012.00	(· , (− , (· , (

						WE	LL NUMBER BH23-04
	NATT	•					PAGE 1 OF 1
Consu	ulting Grou	р					
CLIENT B&A	Planning				PROJE	CT NAME Netook Crossing]
PROJECT NUN	MBER <u>3903</u>	.T01			PROJE	CT LOCATION Netook	
						LEVATION _ 1018.3 m	HOLE SIZE 6" Auger
		k Mounted Auger					
							/ 1016.30 m
			1		÷ A II		
DEPTH (m) SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL	DESCRIPTION	WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
			ОН		(OH) Topsoil		1018.05
	4-6-9 (15)	MC = 16% MC = 17%	CL- ML		(CL-ML) Silty clay ti plastic, brown to gre	II, trace sand. Low to mediun sy, damp, stiff to very stiff. o rock or large boulder.	
					Bottom	of hole at 3.00 m.	

							WE	LL NU	JMBER BH23-05
		VAT T							PAGE 1 OF 1
	_	Iting Grou					DDO IECT NAME Notack Crossing		
	IT <u>B&A I</u> FCT NUM		.T01						
							GROUND ELEVATION 1020.3 m	HOLE S	IZE 6" Auger
							GROUND WATER LEVELS:		
DRILL	ING MET	HOD Truck	k Mounted Auger				AT TIME OF DRILLING		
			CHEC						
NOTE	s			1			_ AFTER DRILLING		
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS		GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
	SPT 1 SPT 2 SPT 2 SPT 3	4-6-8 (14) 5-8-11 (19) 5-8-10 (18) 5-7-13 (20)	MC = 14% MC = 15% MC = 15% MC = 15% MC = 16% MC = 15%	OH CL- ML		(CL-N	Topsoil /L) Silty clay till, trace sand. Low to medium c, brown to grey, damp, stiff to very stiff.	1020.05	
<u> </u>				<u> </u>		5.45	Bottom of hole at 6.45 m.	1013.85	ŀ···;[──-]···;]

BENERAL BH / TP / WELL NETOOK CROSSING.GPJ GINT STD CANADA

								WEI	L NU	MBER BH23-06
		VATT	•							PAGE 1 OF 1
	Consul	ting Group	р							
CLIENT	B&A F	Planning						PROJECT NAME Netook Crossing		
PROJE		BER <u>3903</u>	.T01							
DATES	STARTE	D <u>1/12/23</u>	COMP	LETE	D _1/1	2/23		GROUND ELEVATION 1018.6 m	HOLE SI	ZE _ 6" Auger
DRILLI	NG CON	TRACTOR	Venom Environme	ntal Dr	illing			GROUND WATER LEVELS:		
DRILLI	NG METI	HOD Truck	K Mounted Auger					AT TIME OF DRILLING		
			CHEC							
NOTES								AFTER DRILLING 3.10 m / Elev 1	1015.50 m	
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG			MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН			(OH) To	opsoil		
	SPT 1 SPT 2 SPT 3	4-7-9 (16) 3-6-7 (13) 4-8-15	MC = 14% MC = 16% MC = 16%	CL-			(CL-ML plastic,	.) Silty clay till, trace sand. Low to medium brown to grey, damp, stiff to very stiff.	1018.30	
	SPT	(23) 5-8-12	MC = 16%							
	4	(20)				6.45			1012.15	
								Bottom of hole at 6.45 m.		

			WELL NUMBER BH23-07
	Г		PAGE 1 OF 1
Consulting Grou	lb		
CLIENT B&A Planning			PROJECT NAME Netook Crossing
PROJECT NUMBER 390	3.T01		PROJECT LOCATION Netook
DATE STARTED _2/12/23	3 COMF	PLETED _ 2/1	Image: Market Action
DRILLING CONTRACTOR	Venom Environme		GROUND WATER LEVELS:
DRILLING METHOD			AT TIME OF DRILLING
LOGGED BY GS			
NOTES			
DEPTH (m) (m) sAMPLE TYPE NUMBER BLOW COUNTS (N VALUE)	TESTS	U.S.C.S. GRAPHIC LOG	MATERIAL DESCRIPTION WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
		он	(OH) Topsoil
SPT 3-4-5 	MC = 16%		(CL-ML) Silty clay till, trace sand. Medium plastic, light brown to grey, damp, stiff to very stiff.
SPT 3-6-9 2 (15)	MC = 16%	CL- ML	
	MC = 16%		
SPT 3-5-7 3 (12)			
5	MC = 16%		
	MC = 16%		6.45 1012.05 · · · · · · · ·
			Bottom of hole at 6.45 m.

							WE	ELL NU	MBER BH23-08
									PAGE 1 OF 1
	-	ting Group							
	T <u>B&A P</u>		704						
			.T01						
							GROUND ELEVATION 1018.1 m GROUND WATER LEVELS:		ZE <u>6 Auger</u>
			Mounted Auger						
			CHEC						
							TAFTER DRILLING 2.20 m / Elev	/ 1015.90 m	1
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		(OH) ⁻	Fopsoil	1017.00	
	SPT 2 SPT 3	3-4-6 (10) 3-5-7 (12) 4-6-9 (15) 5-8-10	MC = 16% MC = 18% MC = 17% MC = 16%	CL- ML		(CL-M	L) Silty clay till, trace sand. Low to medium , dark grey, damp, stiff to very stiff.	1017.80	
	4	(18)	MC = 16%			6.45		1011.65	
							Bottom of hole at 6.45 m.		
ō									

VERAL BH / TP / WELL NETOOK CROSSING GPJ GINT STD CANA

							WE	LL NU	JMBER BH23-09
		VATT							PAGE 1 OF 1
	Consu	Iting Group	0						
CLIEN	T B&A	Planning					PROJECT NAME Netook Crossing		
PROJI	ECT NUM	BER 3903	.T01						
DATE	STARTE	D <u>1/12/23</u>		PLETE	D <u>1/1</u>	2/23	GROUND ELEVATION 1019.4 m	HOLES	IZE _ 6" Auger
DRILL	ING CON	TRACTOR	Venom Environme	ntal Dr	illing		GROUND WATER LEVELS:		
DRILL	ING MET	HOD Truck	Mounted Auger						
			CHEC						
NOTE	s						AFTER DRILLING		
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		(OH) 1	opsoil		
						(CL-M	L) Silty clay till, trace sand. Low to medium	1019.10	
L -						plastic	, brown to grey, damp, stiff to very stiff.		
1			MC = 11%						
	SPT	4-6-9							
2		(15)							
L -									
3									
	SPT 2	4-6-10 (16)							
		(10)		CL- ML					
 - 4									
			MC = 15%						
	SPT 3	4-8-9 (17)							
5		. ,	MC = 15%						
<u> </u>									
6				-					
 -	SPT	4-8-10 (18)	MC = 16%						
<u> </u>						6.45	Bottom of hole at 6.45 m.	1012.95	ŀ. ·[⊟·. ·]
QEIN									

Client B&A Planning PROJECT NAME Netook Crossing PROJECT NUMBER 3903.T01 PROJECT LOCATION Netook DATE STARTED 2/12/23 COMPLETED 2/12/23 DRILLING CONTRACTOR Venom Environmental Drilling GROUND ELEVATION 1019.6 m DRILLING METHOD Truck Mounted Auger AT TIME OF DRILLING LOGGED BY GS CHECKED BY JR NOTES Y AFTER DRILLING 4.10 m / Elev 1015.50 m H GUND WATER LEVELS: MATERIAL DESCRIPTION WELL DIAGRA Casing Top (m) MATERIAL DESCRIPTION WELL DIAGRA Casing Top (m) Casing Top (m)				I			WELL NUMBER BH23-10
CLENT B&A Plannina PROJECT NUMBER 2030.101 DATE STARTED 2/12/23 COMPLETED 2/12/23 GROUND ELEVATION 1016 bm DRILLING CONTRACTOR Verom Environmental Dilling DRILLING CONTRACTOR Verom Environmental Dilling DRILLING METHOD Tuck Mounted Auger LOGGED BY GS CHECKED BY JR NOTE CHECKED BY Watter Laves AT TIME OF DRILLING MC CHECKED BY Watter Laves AT TIME OF DRILLING JR MC BROWN WATER LEVELS AT TIME OF DRILLING				1			PAGE 1 OF
PROJECT NUMBER 3303.T01 PROJECT LOCATION Meteode DATE STARTED 2/12/23 COMPLETED 2/12/23 GROUND ELEVATION 1019.6 m HOLE SIZE 6* Auger DRILLING COMPRETOR Venom Environmental Dilling GROUND MATER LEVELS: GROUND MATER LEVELS: AT TIME OF DRILLING	CLIEN	-					PROJECT NAME Netook Crossing
DATE STARTED 2/12/23 COMPLETED 2/12/23 GROUND ALEXATION 1019.6 m HOLE SZE 6" Auger DRILLING CONTRACTOR Truck Mounted Auger							
DRILLING CONTRACTOR Vence Environmental Drilling GROUND WATER LEVELS: LOGGED BY _GS							
DRILLING METHOD Truck Mounted Auger AT TIME OF DRILLING							
NOTES Image: Constraint of the second and graved. Low of the second and graved	DRILLI	NG METI	HOD Truck	Mounted Auger			AT TIME OF DRILLING
$\frac{1}{4} \underbrace{G}_{L} \underbrace{G}_{L} \underbrace{G}_{L} \underbrace{G}_{L} \underbrace{G}_{R} $	LOGGI	ED BY _	GS	CHEC	KED E	BY JF	
OH DH Desc (OH) Topsol 1019.35 1 MC = 10% (CL-ML) Silty day till, trace sand and gravel. Low to medium plastic, brown to grey, damp, stiff to very stiff. 1 MC = 10% - -	NOTES	S					
(CL-ML) Sity clay III, trace sand and gravel. Low to medium plastic, brown to grey, damp, stiff to very stiff.	DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS			Casing Type: 1" PVC
		1 SPT 2 SPT	(11) 4-6-7 (13) 3-5-9	MC = 14% MC = 12% MC = 14%	- CL-		(OH) Topsoil 0.25 (CL-ML) Silty clay till, trace sand and gravel. Low to medium plastic, brown to grey, damp, stiff to very stiff.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	 6 		3-6-11 (17)	MC = 14%	-		

IERAL BH / TP / WELL NETOOK CROSSING GP.L. GINT STD

							WE	LL NU	JMBER BH23-11
		VATT							PAGE 1 OF 1
	Consu	Iting Grou	р						
	T B&A								
			.T01						
							GROUND ELEVATION 1019.5 m	_ HOLE S	ZE 6" Auger
			Mounted Auger				GROUND WATER LEVELS: AT TIME OF DRILLING		
			CHEC						
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		0.20 (OH)	Topsoil	1019.30	
	SPT 1 SPT 2	3-3-6 (9) 3-5-8 (13)	MC = 16% MC = 15% MC = 16%	CL-		(CL-N	IL) Silty clay till, trace sand and gravel. Low dium plastic, brown to grey, damp, stiff to tiff.		
4			MC = 16%	ML		¥			
5	SPT 3	4-5-7 (12)	MC = 16%						
 	SPT	4-7-10	MC = 16%						
<u> </u>	4	(17)				6.45		1013.05	
							Bottom of hole at 6.45 m.		
L									

ERAL BH / TP / WELL NETOOK CROSSING GPJ GINT STD CANA

		WELL	NUMBER BH23-12
			PAGE 1 OF 1
Consulting Group			
CLIENT B&A Planning		PROJECT NAME Netook Crossing	
PROJECT NUMBER 3903.T01		PROJECT LOCATION Netook	
DATE STARTED 2/12/23 COM	PLETED 2/12/23	GROUND ELEVATION 1018.9 m HOL	E SIZE 6" Auger
DRILLING CONTRACTOR Venom Environme	ntal Drilling	GROUND WATER LEVELS:	
DRILLING METHOD Truck Mounted Auger		AT TIME OF DRILLING	
LOGGED BY <u>GS</u> CHEC			
NOTES		AFTER DRILLING	
DEPTH (m) (m) (m) (m) MUMBER COUNTS (N VALUE) (N VALUE)	U.S.C.S. GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1"
	0.1 2000.20		8.70
MC = 14% $MC = 14%$ $MC = 14%$ $MC = 14%$ $MC = 14%$	(CL-M	IL) Silty clay till, trace sand. Low to medium , brown to grey, damp, stiff to very stiff.	
SPT 3-6-10 2 (16) MC = 15%	CL- ML		
MC = 15%			
V SPT 4-6-8			
5			
MC = 14%			
SPT 4-8-11 4 (19) MC = 14%	6 45	404	
	6.45	Bottom of hole at 6.45 m.	2.45[]

Consulting				PAGE 1 OF 1
Consulting	g Group			
CLIENT B&A Plan	ning		PROJECT NAME Netook Crossing	
PROJECT NUMBER	<u>3903.T01</u>		PROJECT LOCATION Netook	
			GROUND ELEVATION 1018.7 m HOLE S	IZE 6" Auger
			GROUND WATER LEVELS:	
	Truck Mounted Auger			
		CKED BY JR		
DEPTH (m) SAMPLE TYPE NUMBER BLOW	SENTRA NAPA NAPA NOO N	U.S.C.S. GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
		OH (OH)	Topsoil	
1 0 2 3 - 3 - 3 - 3 - 3 - 3 - 3	MC = 15% (10) MC = 16% (12) MC = 16%	(CL-M plasti	1018.45 AL) Silty clay till, trace gravel. Low to medium c, brown to grey, damp, stiff to very stiff.	
	(12) MC = 16% MC = 15%	_ CL- ML		
	MC = 14%	⊻		
	-8-12 MC = 16%			
	(20) MC = 18%	6.45	1012.25	
			Bottom of hole at 6.45 m.	

B&A F CT NUM TARTEI	BER <u>3903.</u>							
CT NUM STARTEI NG CON	BER <u>3903.</u>							
STARTEI NG CON		T04				PROJECT NAME Netook Crossing		
NG CON	1/10/02	101				PROJECT LOCATION Netook		
	<u> </u>	COMF	LETE	D _1/12	/23	GROUND ELEVATION 1020.4 m	HOLE S	IZE 6" Auger
	TRACTOR _	Venom Environme	ntal Dr	illing		GROUND WATER LEVELS:		
NG MET	HOD Truck	Mounted Auger				AT TIME OF DRILLING		
D BY _	GS	CHEC	KED E	BY JR				
						AFTER DRILLING		
SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
SPT 1	3-4-6 (10)	MC = 13% MC = 12%	ML		(ML) damp	Silty sand, trace clay and gravel. Brown, o, compact, low plasticity.	1020.20	
SPT 2	3-5-7 (12)	MC = 11% MC = 12%			(CL-I to me	viL) Siity clay till, trace sand and gravel. Low edium plastic, dark grey, damp, very stiff.		
SPT 3	4-7-9 (16)	MC = 12%	CL- ML					
SPT 4	5-8-12 (20)	MC = 14%			45	Bottom of hole at 6.45 m.	1013.95	
	SAMPLE TYPE SAMPLE	BAFE TYPE SMPLE TYPE S	MAL BAY MOTE MOTE TESTS MOTE MC = 13% MC = 13% MC = 13% SPT 3-4-6 (10) MC = 12% SPT 3-5-7 (12) MC = 11% SPT 3-5-7 (12) MC = 12% SPT 3-5-7 (12) MC = 12% SPT 5-8-12 MC = 12%	ВАН ВИ ВО ОХУ TESTS OH MO BO OXY MC = 13% ML SPT 3-4-6 (10) MC = 13% ML SPT 3-4-6 (10) MC = 12% ML SPT 3-5-7 (12) MC = 11% ML SPT 3-5-7 (12) MC = 12% CL- SPT 4-7-9 (16) MC = 12% CL- SPT 5-8-12 MC = 14% CL-	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	But grand Matterial Description TESTS 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

GP.J GINT CROSSING 200 GENERAL BH / TP / WELL NET

							WE	LL NU	JMBER BH23-15
		VATT							PAGE 1 OF 1
	_	Iting Group							
	T <u>B&A</u>		T01						
			.T01						
							_ GROUND ELEVATION _1019.5 m _ GROUND WATER LEVELS:		IZE <u>6 Auger</u>
			Mounted Auger						
			CHEC						
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		(OH)	Topsoil	1010 20	
 			MC = 14%	ML		(ML)	Silty sand, trace clay and gravel. Brown, o, compact, low plasticity.	1019.20	
 3	SPT 1	4-8-10 (18)	MC = 13%		2222				
	SPT 2	3-7-10 (17)	MC = 15%	_		to m	ML) Silty clay till, trace sand and gravel. Low edium plastic, dark grey, damp, very stiff.		
			MC = 14%						
5	SPT 3	4-8-9 (17)	MC = 15%	CL- ML					
	SPT 4	5-9-14 (23)	MC = 15%	_		6.45		1013.05	
							Bottom of hole at 6.45 m.		

							WELL N	UMBER BH23-16
		ΥΑΤΤ						PAGE 1 OF 1
	Consul	ting Group)					
CLIEN	F <u>B&A</u> I	Planning					PROJECT NAME _ Netook Crossing	
			.T01					
							GROUND ELEVATION 1019.6 m HOLE	SIZE 6" Auger
							GROUND WATER LEVELS:	
			Mounted Auger					
			CHEC					
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
	SPT 1 SPT 2	3-5-6 (11) 3-6-7 (13) 3-6-11	MC = 10% MC = 13% MC = 14%	OH CL- ML		(CL-N	Topsoil IL) Silty clay till, trace gravel. Low to medium , brown to grey, damp, stiff to very stiff.	
5	SPT 3	3-6-11 (17)	MC = 14%	_		¥		
<u> </u>	4	(17)				6.45	1013.1	5
							Bottom of hole at 6.45 m.	

PROJECT NUMBER <u>3903.T</u> DATE STARTED <u>1/12/23</u> DRILLING CONTRACTOR <u>V</u> DRILLING METHOD <u>Truck</u> LOGGED BY <u>GS</u> NOTES	T01 COMF Venom Environme Mounted Auger CHEC	PLETE ntal Dr	D <u>1/12/23</u> illing 3Y JR	PROJECT NAME <u>Netook Crossing</u> PROJECT LOCATION <u>Netook</u> GROUND ELEVATION <u>1018.8 m</u> GROUND WATER LEVELS: AT TIME OF DRILLING AT END OF DRILLING	
DEPTH (m) (m) SAMPLE TYPE NUMBER BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
$\begin{array}{c} & & \\$	MC = 13% MC = 15% MC = 15% MC = 15% MC = 14%	OH ML	0.30 (ML dam) Topsoil) Silty sand, trace clay and gravel. Brown, p, compact, low to medium plasticity.	1018.50
SPT 5-7-12 4 (19)	MC = 16%		6.45	Bottom of hole at 6.45 m.	1012.35

GP.J GINT CROSSING 200 GENERAL BH / TP / WELL NET

		VAT T					WEL	L NU	JMBER BH23-18 PAGE 1 OF 1
	Consu	Iting Group)						
CLIEN	IT <u>B&A</u> I	Planning					PROJECT NAME Netook Crossing		
PROJE	ECT NUM	BER <u>3903.</u>	T01				PROJECT LOCATION Netook		
DATE	STARTE	D 1/12/23	COMF	PLETE	D _1/*	12/23	GROUND ELEVATION 1019.5 m	HOLE S	IZE 6" Auger
DRILL	ING CON		Venom Environme	ntal Dr	rilling		GROUND WATER LEVELS:		
DRILL	ING MET	HOD Truck	Mounted Auger				AT TIME OF DRILLING		
LOGG	ED BY	GS	CHEC	KED I	BY JF	२	AT END OF DRILLING		
NOTE	s						AFTER DRILLING		
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
	-			ОН			Topsoil	4040.00	
 - 1 2 	SPT 1	4-8-10 (18)	MC = 12% MC = 14%	ML		plastic 1.50 (CL-N	Silty sand, trace clay. Brown, damp, stiff, low ity. IL) Silty clay till, trace sand and gravel. Low dium plastic, light grey, damp, very stiff.	<u>1019.20</u> <u>1018.00</u>	
	SPT 2	5-8-9 (17)	MC = 15% MC = 14%	CL- ML					
	SPT 3	5-8-10 (18)	MC = 15%						
6	SPT 4	5-8-11 (19)	MC = 14%			6.45	Bottom of hole at 6.45 m.	1013.05	

							WEI	L NU	JMBER BH23-19 PAGE 1 OF 1
		ting Group	1						PAGE I OF I
CLIEN	T B&A I						PROJECT NAME Netook Crossing		
			.T01						
							GROUND ELEVATION 1018.3 m	HOLE S	IZE _6" Auger
DRILLI	NG CON	TRACTOR	Venom Environme	ental Dr	illing		GROUND WATER LEVELS:		
DRILLI	NG MET	HOD Truck	Mounted Auger				AT TIME OF DRILLING		
LOGGI	ED BY	GS	CHEC	KED E	BY JF	र			
NOTES	S						TAFTER DRILLING 3.90 m / Elev 7	1014.40 m	1
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		(OH) 0.25	Topsoil	1018.05	
 - 1 			MC = 15%	ML		(ML) \$ damp, 1.50	Silty sand, some gravel, trace clay. Brown, compact, low plasticity.	1016.80	
 3	SPT 1	4-6-9 (15)	MC = 10%	_		(CL-M plastic	IL) Silty clay till, trace gravel. Low to medium , light grey, damp, very stiff.		
	SPT 2	3-5-7 (12)	MC = 11%						
 			MC = 11%	CL- ML		Ţ			
 	SPT 3	3-5-13 (18)	MC = 11%						
 6 	SPT 4	3-6-10 (16)	MC = 14%	_		6.45	Bottom of hole at 6.45 m.	1011.85	

ERAL BH / TP / WELL NETOOK CROSSING.GPJ GINT STD CANADA

		ATT ting Group						WEL	L NU	JMBER BH23-20 PAGE 1 OF 1		
CLIEN	- T_B&AF							PROJECT NAME Netook Crossing				
			T01									
								GROUND ELEVATION 1019.9 m				
								GROUND WATER LEVELS:				
			Mounted Auger									
			CHEC	KED E	B Y _JF	२						
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG			MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev:		
	l'S									Casing Type: 1" PVC		
				OH		0.20		Topsoil	1019.70			
			MC = 9%	ML		1.50	damp,	Silty sand, some gravel, trace clay. Brown, , compact, low plasticity.	1018.40			
 	SPT 1	3-5-7 (12)	MC = 13%				(CL-M	IL) Silty clay till, trace gravel. Low to medium b, brown to grey, damp, stiff to very stiff.				
	SPT 2	4-7-9 (16)	MC = 12%									
			MC = 9%	CL- ML								
 	SPT 3	4-8-10 (18)	MC = 9%			Ţ						
6	SPT 4	10-16-16 (32)	MC = 6%	-		6 45			1012 45			
		I		1		<u> 6.45</u>		Bottom of hole at 6.45 m.	1013.45	r• u - r• u		

AL BH / TP / WELL NETOOK CROSSING.GPJ GINT S

	Consul IT <u>B&A I</u>		T01				PROJECT NAME Netook Crossing	
							GROUND ELEVATION _1019.4 m	
							GROUND WATER LEVELS:	
			Mounted Auger					
LOGG	ED BY	GS	CHEC	KED E	BY _JF	۲		
NOTE	s						AFTER DRILLING 5.00 m / Elev	1014.40 m
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		0.25	OH) Topsoil	1019.15
 _ 1 	-		MC = 11%	ML		((d	ML) Silty sand, some gravel, trace clay. Brown, lamp, compact, low plasticity.	
	SPT 1	3-3-7 (10)	MC = 11%			((tc	CL-ML) Silty clay till, trace sand and gravel. Low o medium plastic, brown, damp, stiff to very stiff.	
· _	SPT 2	3-5-11 (16)	MC = 17%					
4			MC = 12%	CL- ML				
	SPT 3	4-6-9 (15)	MC = 13%			Ā		
- - - 6	SPT 4	3-8-11 (19)	MC = 19%	-				
		-				6.45	Bottom of hole at 6 45 m	1012.95
		3-8-11 (19)	MC = 19%			6.45	Bottom of hole at 6.45 m.	1012.95

							WE	LL NU	JMBER BH23-22
		VATT	•						PAGE 1 OF 1
	Consu	Iting Grou	р						
CLIEN	T_B&A	Planning					PROJECT NAMENetook Crossing		
PROJE	ECT NUM	BER <u>3903</u>	.T01				PROJECT LOCATION Netook		
DATE	STARTE	D 1/12/23	COMF	LETE	D _1/	12/23	GROUND ELEVATION 1018.2 m	HOLE S	IZE _ 6" Auger
DRILL	ING CON	TRACTOR	Venom Environme	ntal Dr	illing		GROUND WATER LEVELS:		
DRILL	ING MET	HOD Truck	K Mounted Auger				AT TIME OF DRILLING		
			CHEC						
NOTE	S						AFTER DRILLING		
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
	SPT 1 SPT 2 SPT 3	3-4-5 (9) 4-6-7 (13) 3-5-8 (13) 3-7-8 (15)	MC = 15% MC = 16% MC = 17% MC = 16% MC = 14%	OH CL- ML		(CL-M Mediu	Topsoil AL) Silty clay till, trace gravel and sand. Im plastic, brown, damp, stiff to very stiff.	1017.95	
			1	<u> </u>	иш	6.45	Bottom of hole at 6.45 m.	1011.75	
j									

		ν Α ΤΤ					WE	LL NU	JMBER BH23-23 PAGE 1 OF 1
		Iting Group							
CLIEN	T B&A	Planning					PROJECT NAME Netook Crossing		
			.T01						
DATE	STARTE	D <u>1/12/23</u>		LETE	D _1/*	12/23	GROUND ELEVATION 1018.9 m	HOLE S	IZE _ 6" Auger
							GROUND WATER LEVELS:		
DRILL	ING MET	HOD Truck	Mounted Auger				AT TIME OF DRILLING		
LOGG	ED BY	GS	CHEC		BY _JF	2			
NOTE	s						_ AFTER DRILLING		
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS		GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		0.20 (OH)	Topsoil Silty sand, trace clay. Brown, damp, stiff, low	1018.70	
						(IVIL) plasti			
	-								
	-			ML					
1			MC = 12%						
	-								
	-					1.50		1017.40	
	SPT	3-3-7				(CL-N	/IL) Silty clay till, trace gravel. Low to medium c, brown to grey, damp, stiff to very stiff.	1	
		(10)				plasu	c, brown to grey, damp, suit to very suit.		
2	-		MC = 16%						
	-								
	-								
	-								
	-								
3				-					
	SPT 2	3-5-10 (15)	MC = 16%						
		(13)							
	-								
	-								
4	-		MC = 16%	CL- ML					
	-								
	SPT	4-8-9							
;	3	(17)							
5			MC = 16%						
}									
;									
- - -									
6				-					
	SPT	5-8-13 (21)	MC = 17%						
		(= ·)			HHH	6.45	Bottom of hole at 6.45 m.	1012.45	
r r							Bollom of hole at 0.43 m.		

		VATT	I				WEL	L NU	JMBER BH23-24 PAGE 1 OF 1
	Consul	ting Group)						
CLIEN	T B&A F	Planning					PROJECT NAMENetook Crossing		
PROJE	ECT NUM		.T01						
DATE	STARTE	D <u>1/12/23</u>		LETE	D _1/*	12/23	GROUND ELEVATION 1019.3 m	HOLE S	IZE 6" Auger
DRILL			Venom Environme	ntal Dr	illing		GROUND WATER LEVELS:		
DRILL		HOD Truck	Mounted Auger				AT TIME OF DRILLING		
LOGG	ED BY	GS	CHEC	KED E	BY JF	र	AT END OF DRILLING		
NOTES	s						AFTER DRILLING		
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		(OH) 0.25	Topsoil	1019.05	
	SPT 1 SPT 2	4-5-7 (12) 4-6-9 (15)	MC = 14% MC = 14% MC = 15%	ML		(ML) ; plastic 1.50 (CL-N	Silty sand, trace clay. Brown, damp, stiff, low ity. IL) Silty clay till, trace gravel. Low to medium ;, brown to grey, damp, stiff to very stiff.	1019.05	
 			MC = 15%	CL- ML					
 5	SPT 3	5-6-8 (14)	MC = 15%						
	SPT 4	8-8-10 (18)	MC = 15%	-		6.45	Bottom of hole at 6.45 m.	1012.85	

							WE	LL NU	MBER BH23-25
			-						PAGE 1 OF 1
CLIENT	B&A F	Iting Group					PROJECT NAME _ Netook Crossing		
			.T01						
							GROUND ELEVATION 1018.5 m		
							GROUND WATER LEVELS:		
			Mounted Auger						
LOGGE	DBY _	GS	CHEC	KED E	BY JF	R			
NOTES							T AFTER DRILLING 4.70 m / Elev	1013.80 m	
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		(OH) ⁻	Fopsoil	1018 20	
	SPT 1 SPT 2	4-6-8 (14) 4-5-6 (11)	MC = 13% MC = 12% MC = 15%	CL-		(CL-N	L) Silty clay till, trace sand. Medium plastic, to grey, damp, stiff to very stiff.	1018.20	
			MC = 15%	- ML					
5	SPT 3	3-6-11 (17)	MC = 15%			Ţ		- - - - -	
	SPT 4	3-6-10 (16)	MC = 15%	-		6.45		1042.05	
				1	иий	6.45	Bottom of hole at 6.45 m.	1012.05	·· :[· .]

		VAT T Iting Group					WE	LL NU	PAGE 1 OF 1
	NT <u>B&A</u> I								
			T01						
							GROUND ELEVATION 1018 m	HOLE SI	ZE 6" Auger
							GROUND WATER LEVELS:		
			Mounted Auger						
			CHEC						
NOTE	S	1		1	1	I	AFTER DRILLING		
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
 1 	-		MC = 15%	OH		(ML) comp	Topsoil Silty sand, trace clay. Brown, damp, loose to act, low plasticity.		
 3	SPT 1	3-4-6 (10)	MC = 16%			1.50 (CL-M to me stiff.	/IL) Silty clay till, trace sand and gravel. Low dium plastic, dark grey, damp, stiff to very	1016.50	
	SPT 2	3-5-8 (13)	MC = 16%	-					
 _4	-		MC = 16%	CL- ML				- - - - -	
 _ 5	SPT 3	4-6-8 (14)	MC = 16%						
	SPT 4	5-8-9 (17)	MC = 16%	-		6.45	Bottom of hole at 6.45 m.	1011.55	

		VAT T					WE	LL NU	JMBER BH23-27 PAGE 1 OF 1
	-	Iting Group							
	T <u>B&A I</u>		T01						
							GROUND ELEVATION 1019 m		
									IZE <u>6 Auger</u>
			Mounted Auger				GROUND WATER LEVELS:		
			CHEC						
DEPTH (m)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM Casing Top Elev: (m) Casing Type: 1" PVC
				ОН		(OH) 0.25	Topsoil	1018.75	
 	SPT 1	3-4-6 (10)	MC = 13%	ML		(ML) damp 1.50 (CL-N	Silty sand, trace clay and gravel. Light brown , stiff, low plasticity. //L) Silty clay till, trace sand. Low to medium c, dark grey, damp, stiff to very stiff.	n, 1017.50	
 3			MC = 14%						
	SPT 2	3-6-8 (14)	MC = 16%	-					
			MC = 16%	CL- ML					
 5	SPT 3	4-7-9 (16)	MC = 16%						
 6	SPT 4	5-8-11 (19)	MC = 15%	-					
				<u> </u>		6.45	Bottom of hole at 6.45 m.	1012.55	k(−]